



Master in Electrical and Electronics Engineering

EE-517: Bio-Nano-Chip Design

Lecture #4

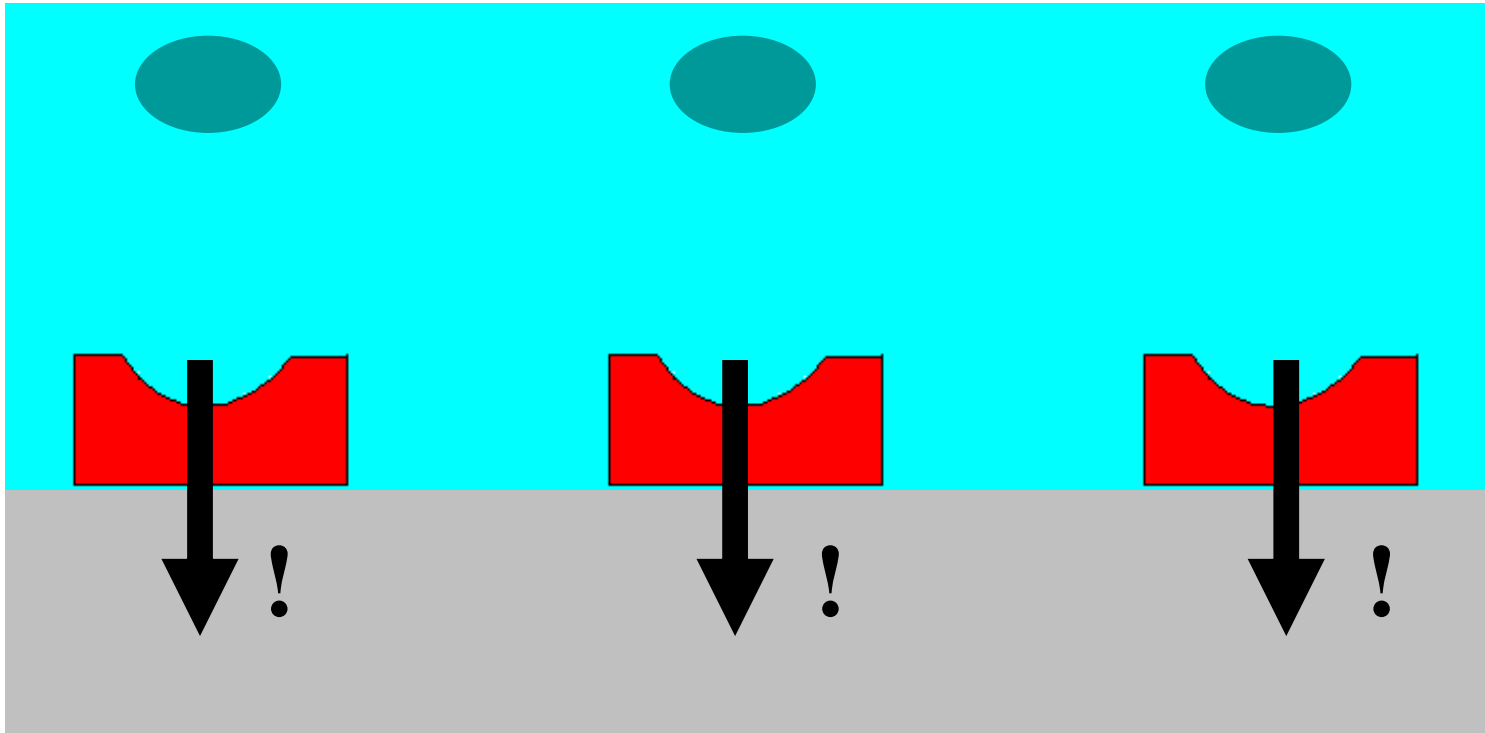
Probe Detection Principles (Faradaic Processes)

Lecture Outline

(Book Bio/CMOS: Chapter' paragraphs § 8.2 & 8.5-8)

- Electrochemical interfaces with enzymes
- Faradaic currents at the interface
- Electrochemical cells and equivalent circuits
- Calibration curve, Sensitivity, and LOD

CMOS/Sample interface



We may exploit some catalyzed reactions with transfer of electrons for detection aims at our Bio/CMOS interfaces



Q1

Recall:

What is a catalyst?

- A.** A molecule accelerating chemical reactions
- B. A molecule accelerating only biochemical reactions
- C. A biomolecule accelerating chemical reactions
- D. A molecule accelerating only redox reactions



Q2

Recall:

What is an enzyme?

- A. An organic molecule
- B. A protein
- C. A DNA sequence
- D. A catalyst
- ☒ E. A biological catalyst



Q3

What is a Redox Enzyme?

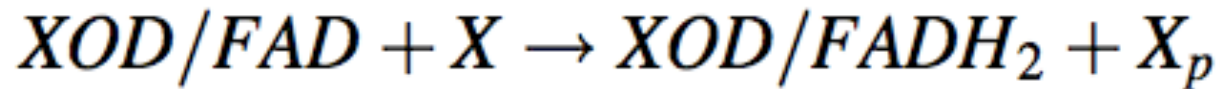
- A. An enzyme that accelerates only Oxidations
- B. An enzyme that accelerates only Reductions
- ☒ C. An enzyme that involves transfer of electrons between chemical species
- ☒ D. An enzyme that catalyzes oxidation-reduction reactions

Enzymes' based detection

In the case of some enzymes, we can easily exploit the redox reactions involving their substrates to the aim of electrochemical direct detection: e.g., that's the case of oxidases and cytochromes.

Redox with oxidases

The typical redox involving an oxidase is as follows:

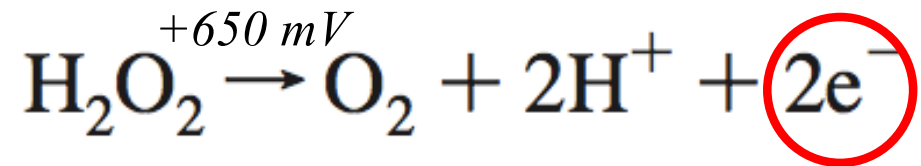


The FAD (Flavin Adenine Dinucleotide) is a functional part of the protein that gains a hydrogen molecule after the reaction. Therefore, the oxidase is not yet ready for another transformation because the FAD has gained the H₂. To return to its initial state, the enzyme needs to release that hydrogen molecule:

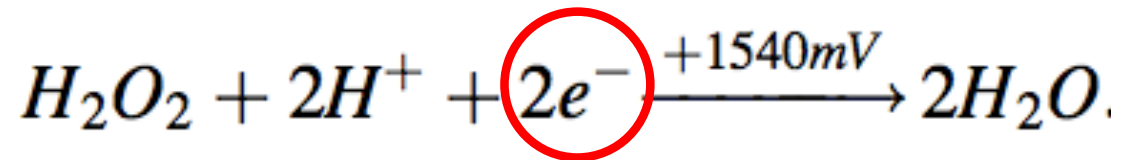


Redox with oxidases

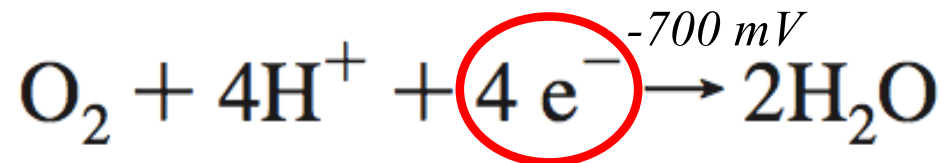
The hydrogen peroxide provide two possible redox reactions. An oxidation:



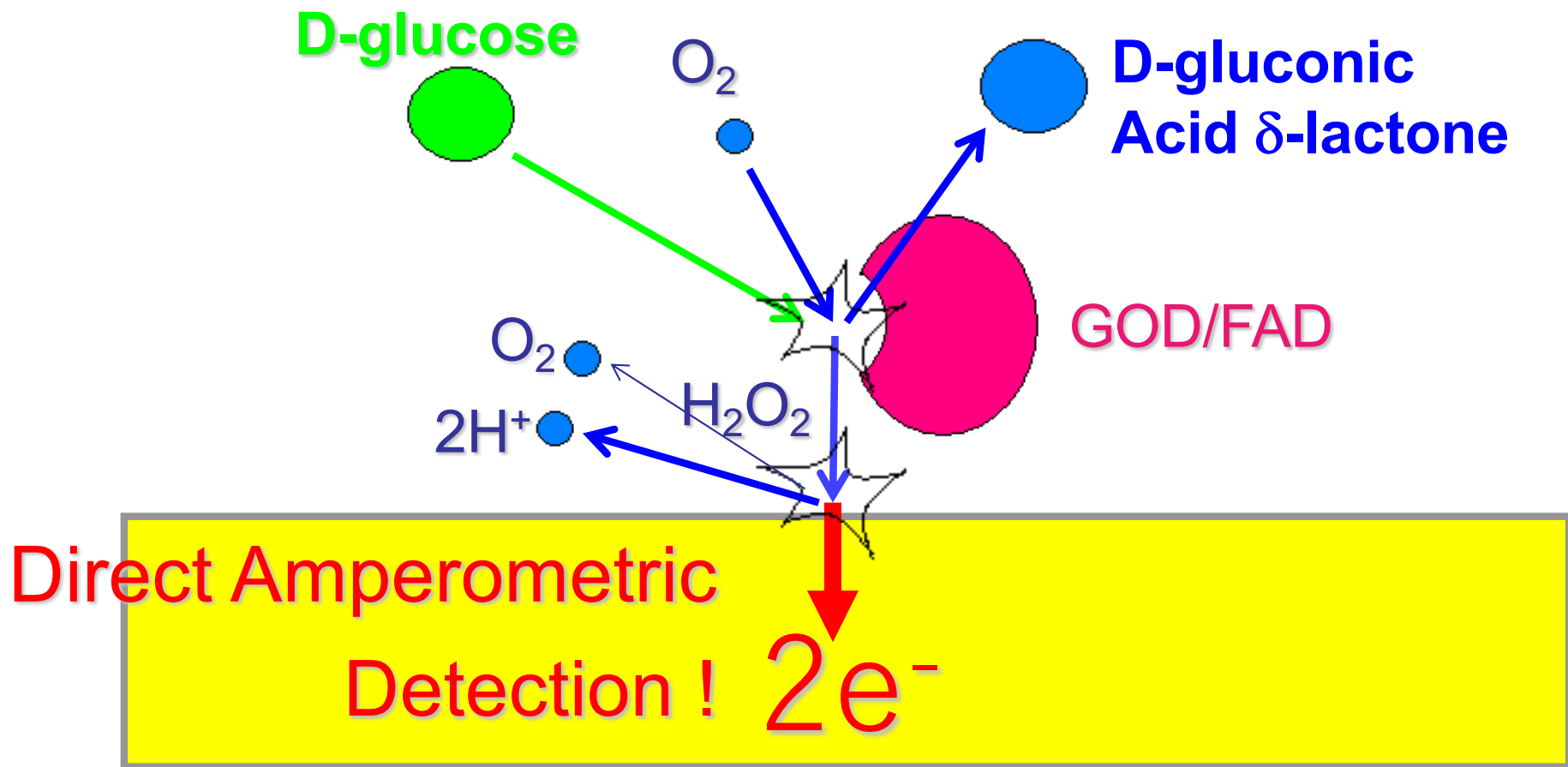
And a reduction:



A third redox is provided by the oxygen reduction:



Oxidases based detection



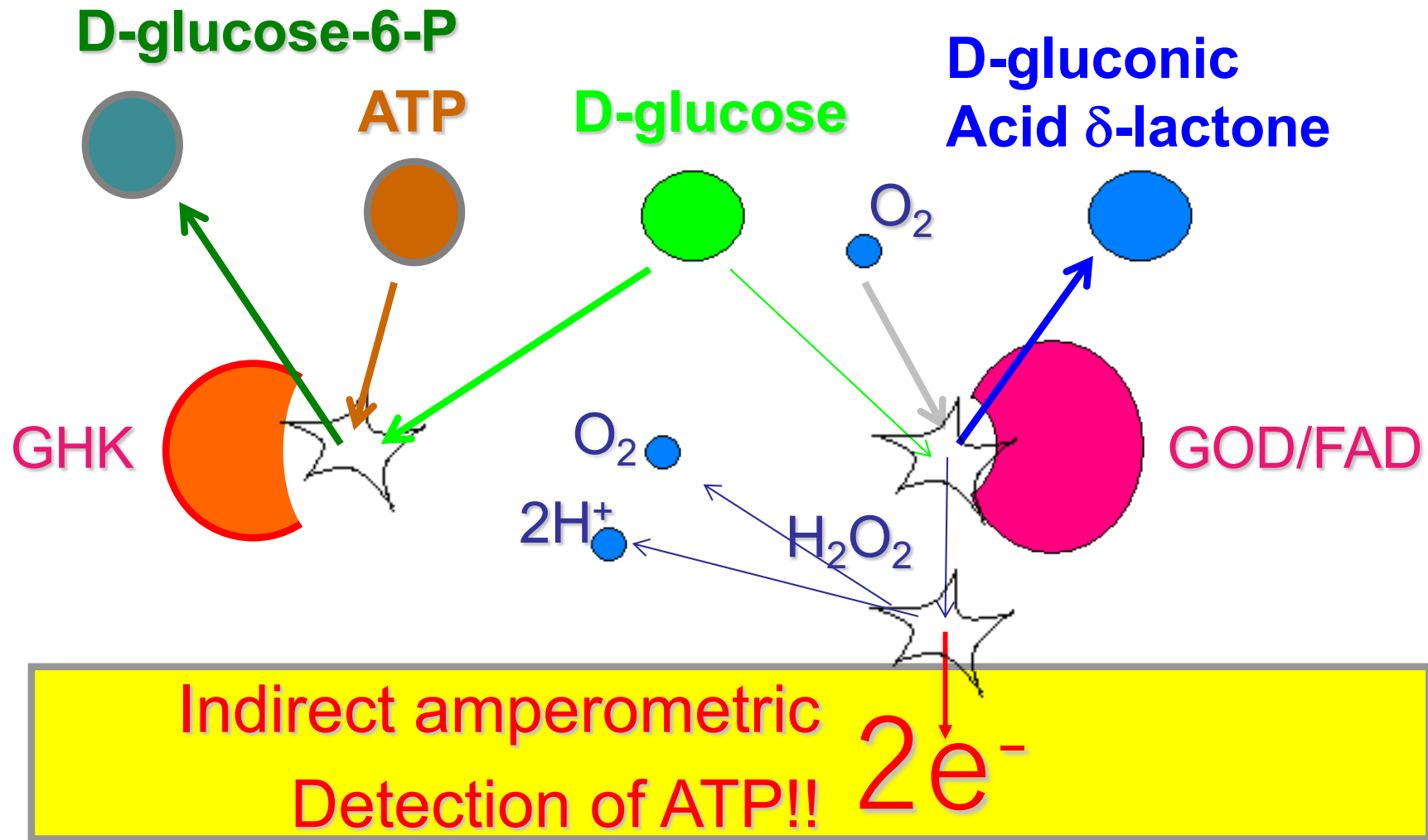


Q4

All the enzyme transfer electrons among species?

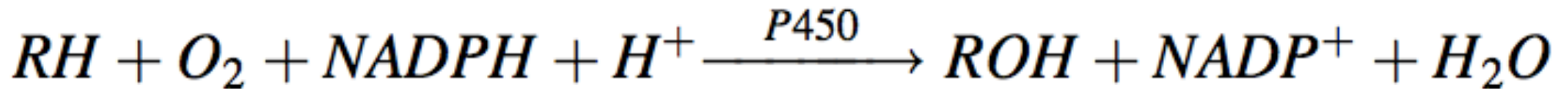
- ☒ A. Yes, of course!
- ☒ B. Only redox enzymes
- C. No, only biological enzymes
- D. No, only oxidases
- E. No, only oxidases and cytochromes

ATP detection

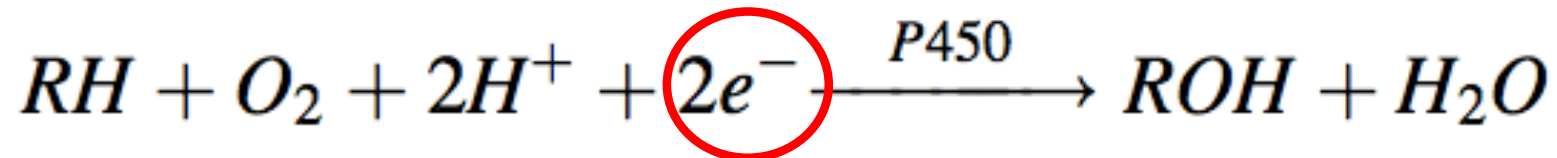


Redox with P450

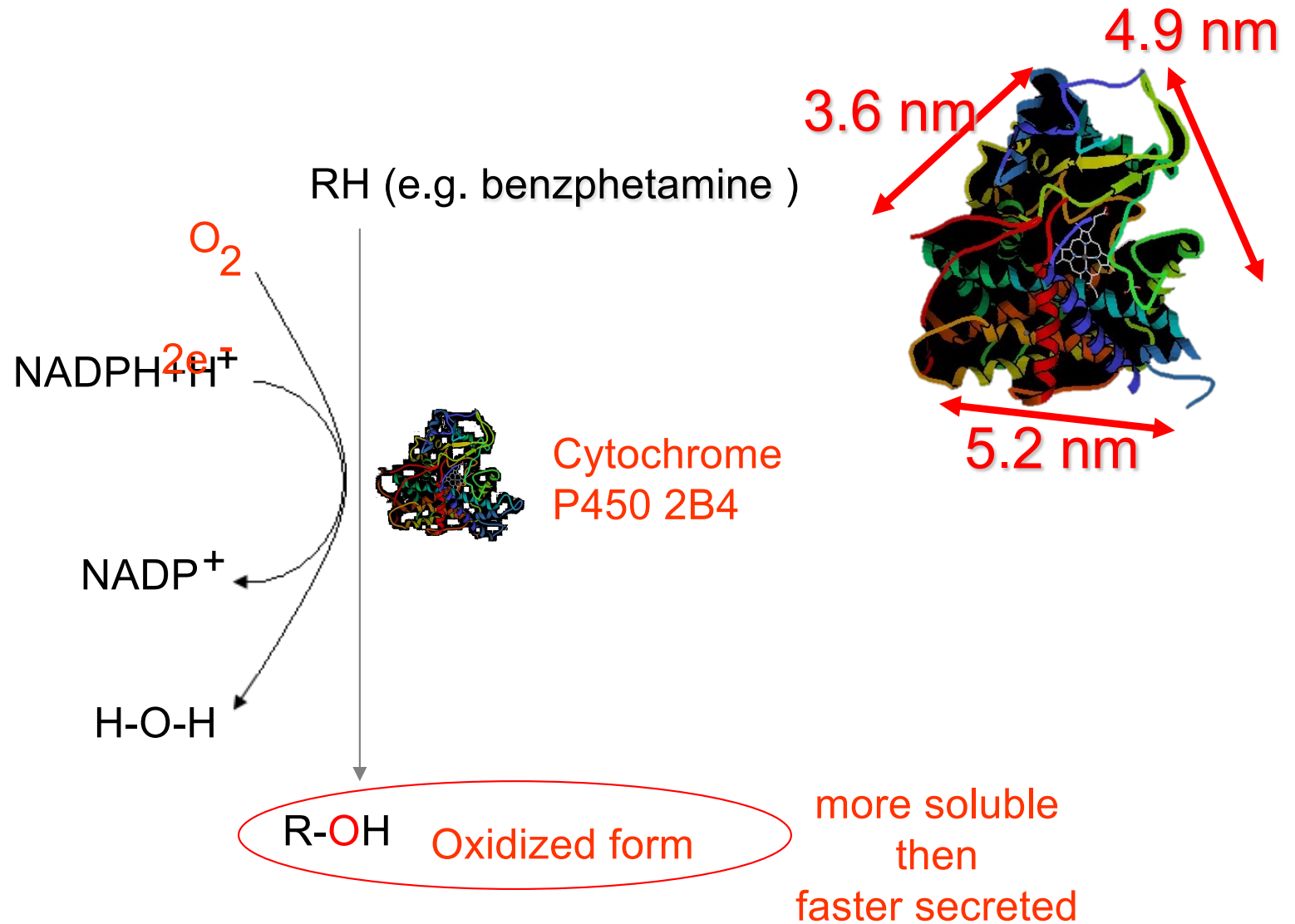
The typical redox involving a cytochrome P450 is as follows:



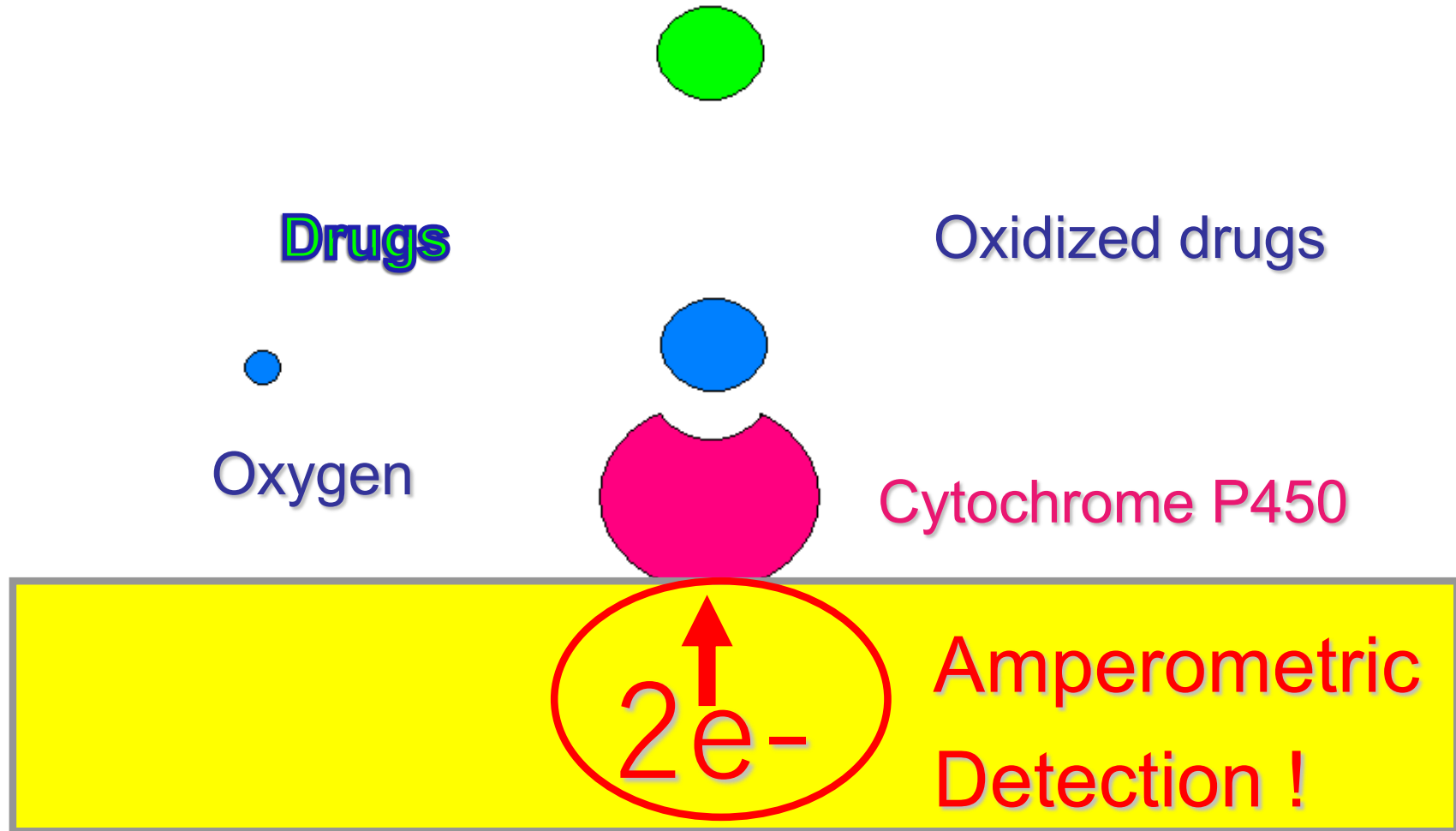
The coenzyme NADPH is mainly providing the need for two electrons required by the drug transformation. Without NADPH, the reaction occurs in water solution using hydrogen ions by water but need two extra electrons:



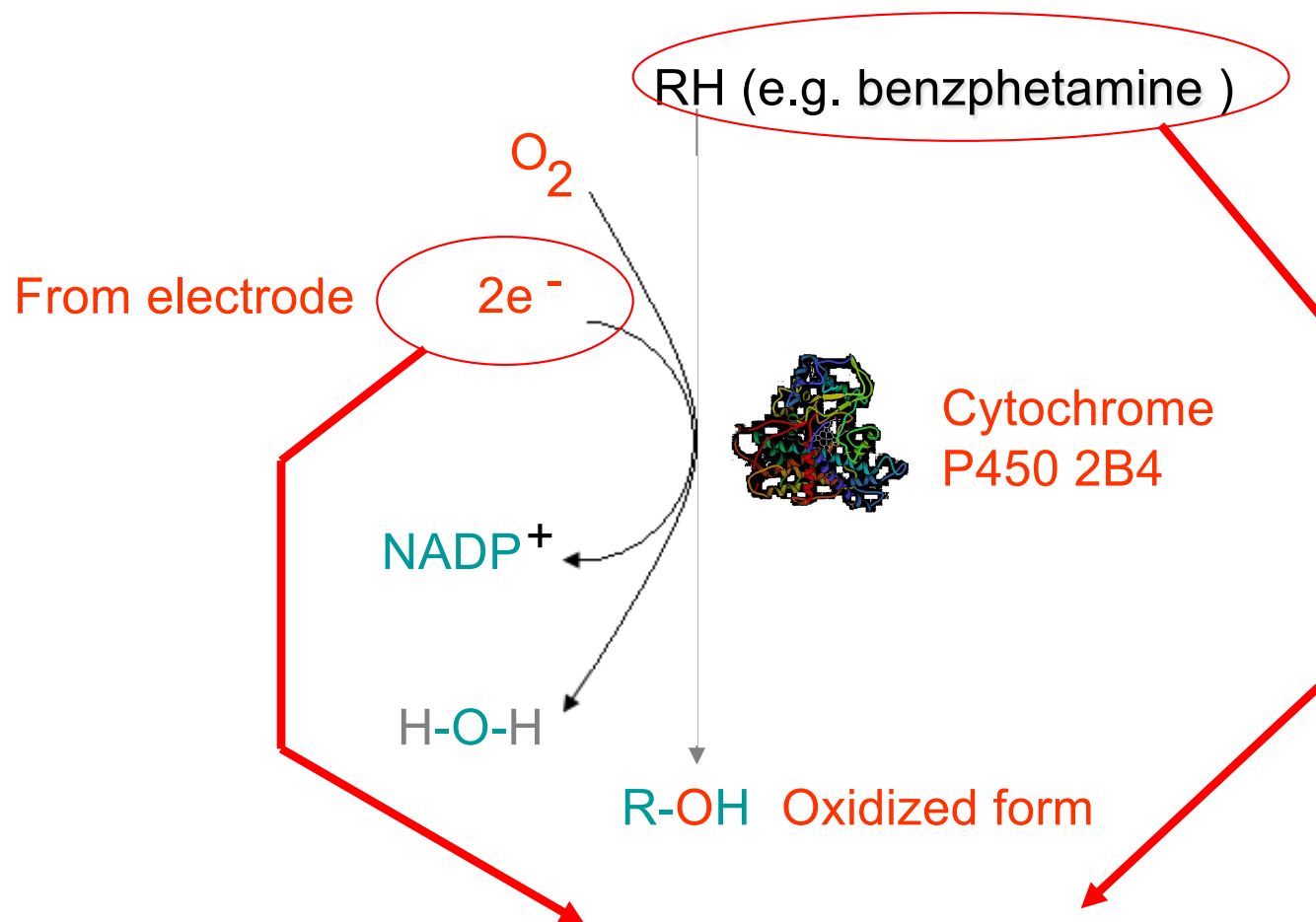
P450 working Principle



P450-based Detection

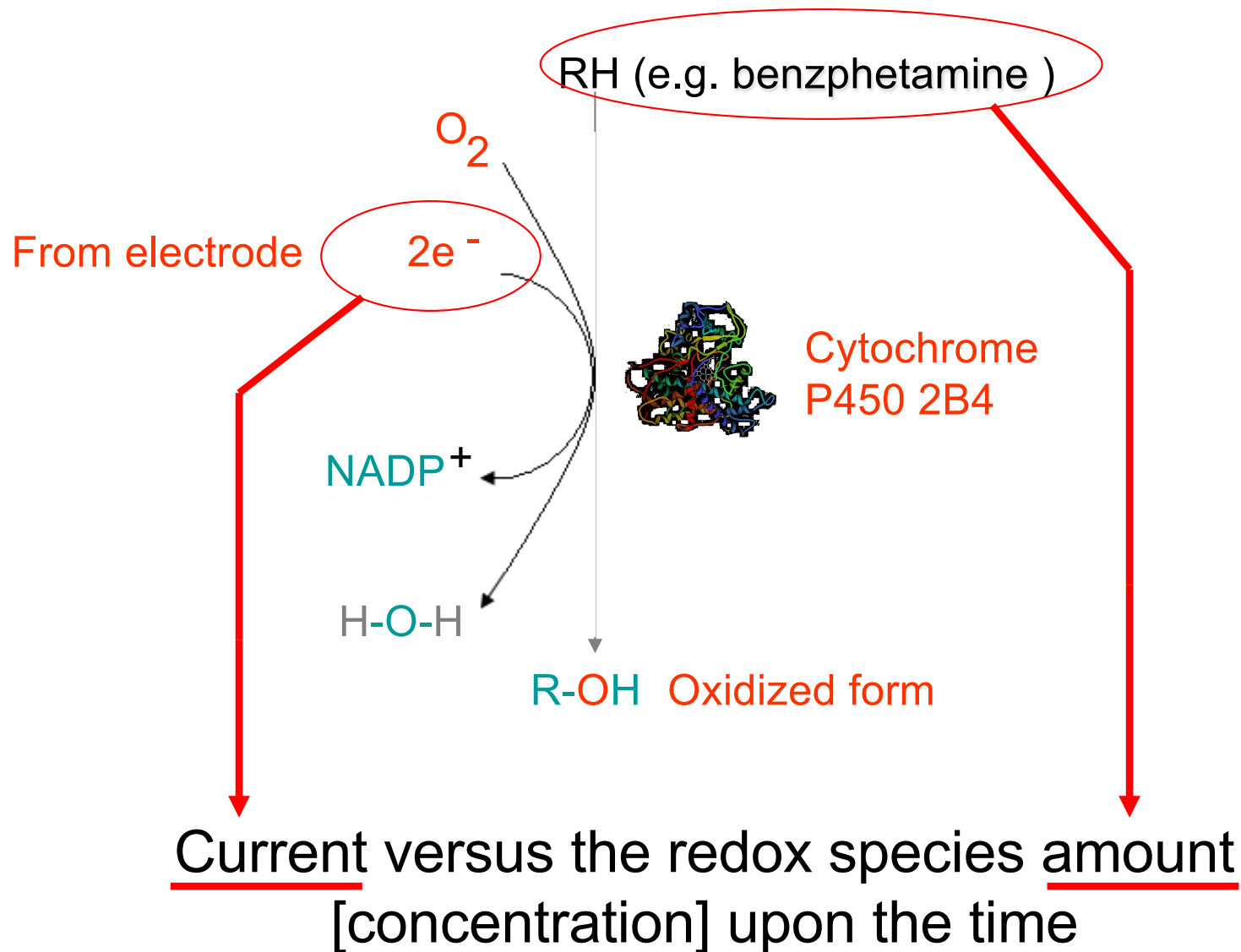


Enzyme based Detection



What's about the electro-CHEMICAL properties?

Enzyme based Detection





Q5

How many electrodes are required to measure at best a current vs a redox?

A. 1

B. 2

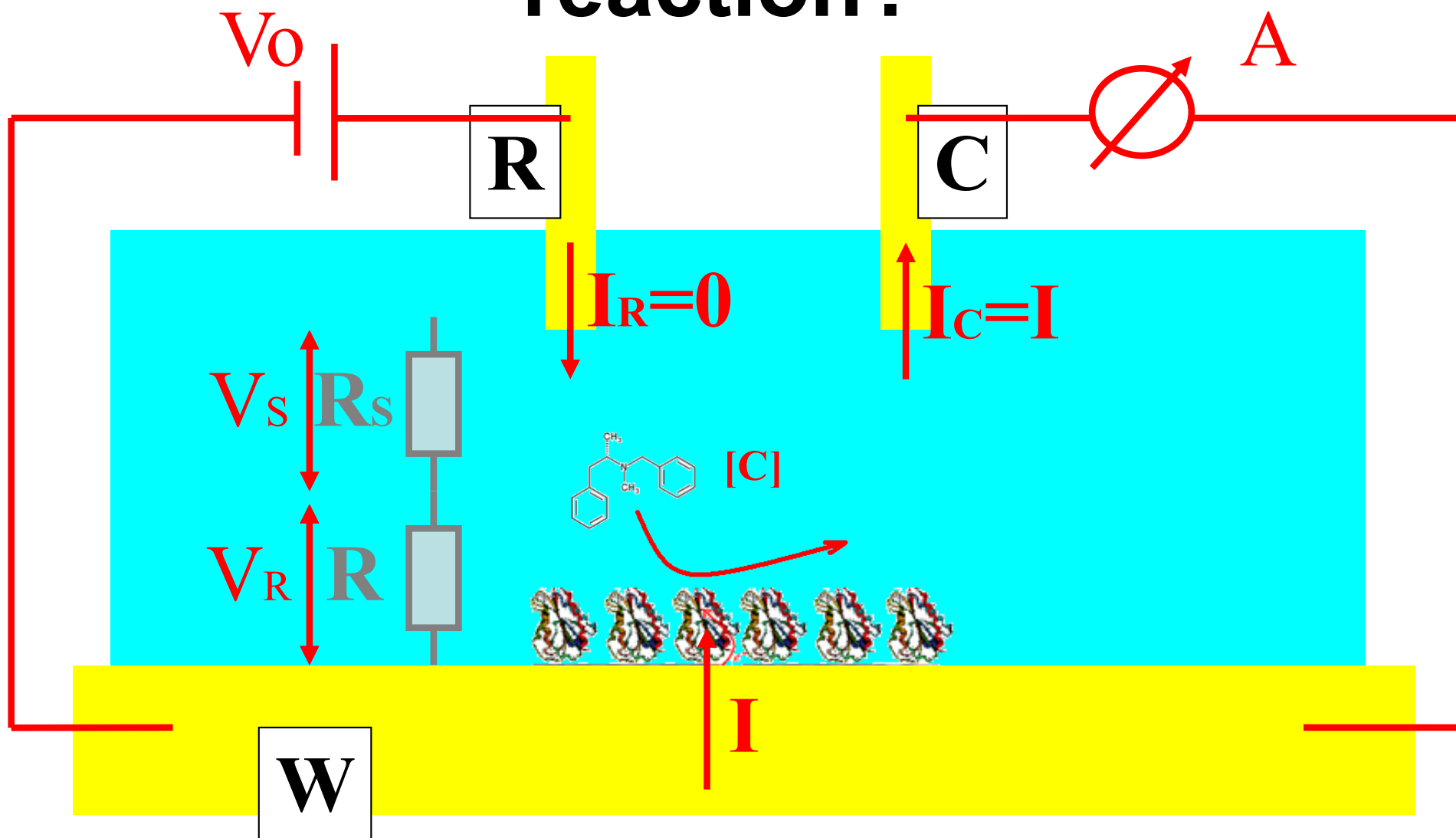
C. 3

D. 4

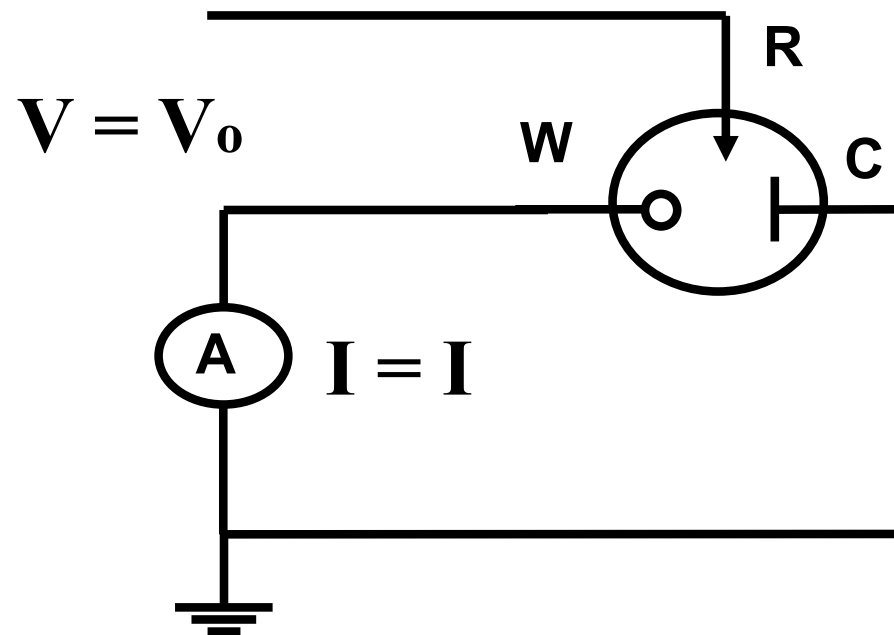
E. 5

F. 5+

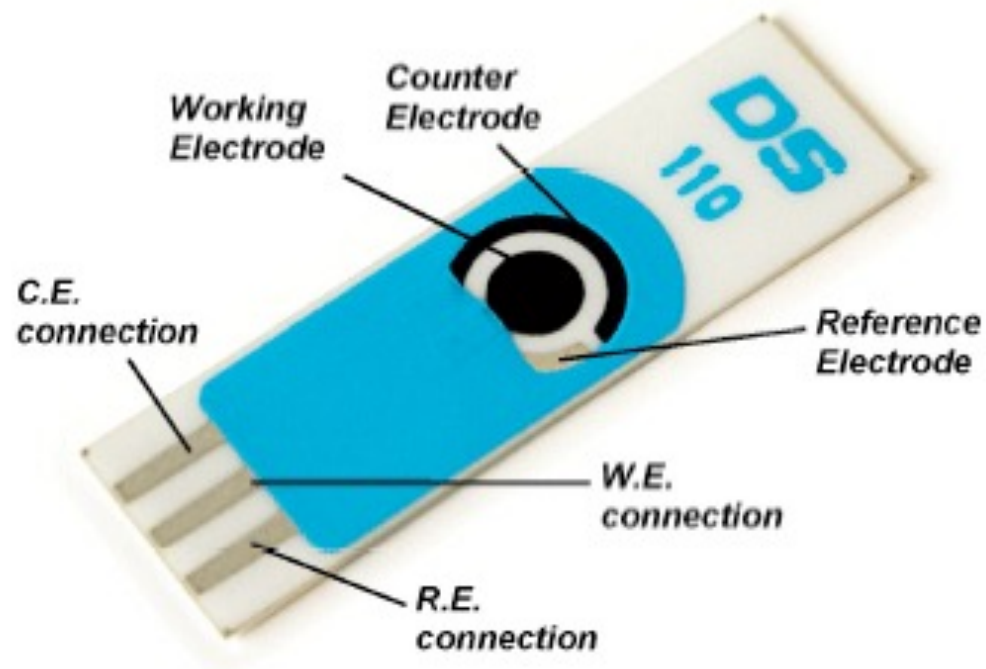
How to measure a redox reaction?



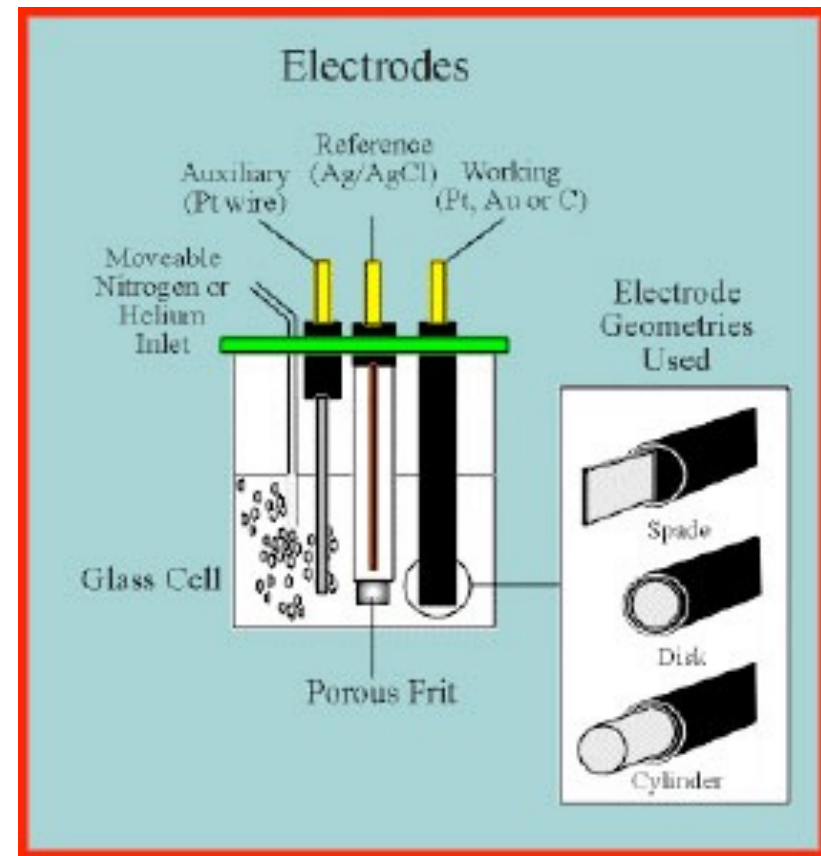
The three-electrode Electrochemical cell



The three-electrode Electrochemical cell



Different kinds of three-electrode Electrochemical cell





Q6

How many electrodes might have an electrochemical cell?

A. 1

B. 2

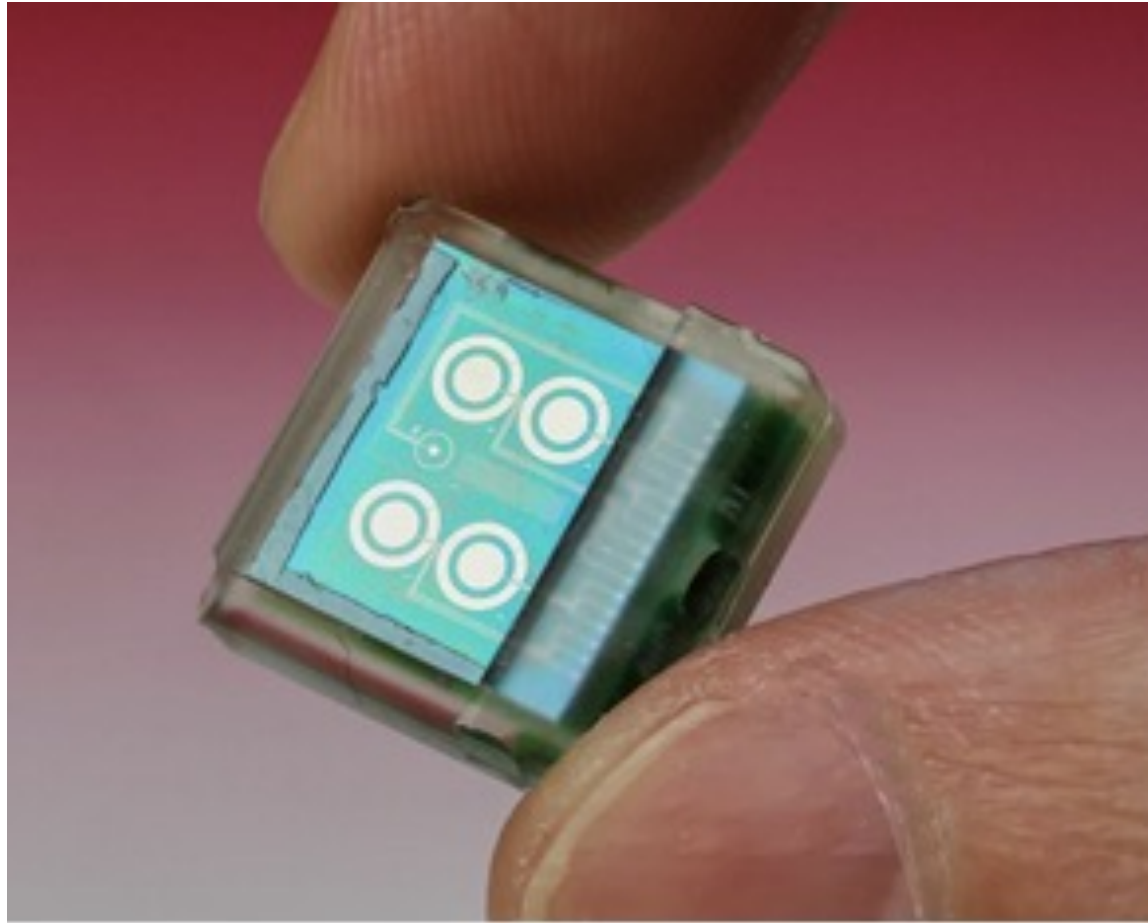
C. 3

D. 4

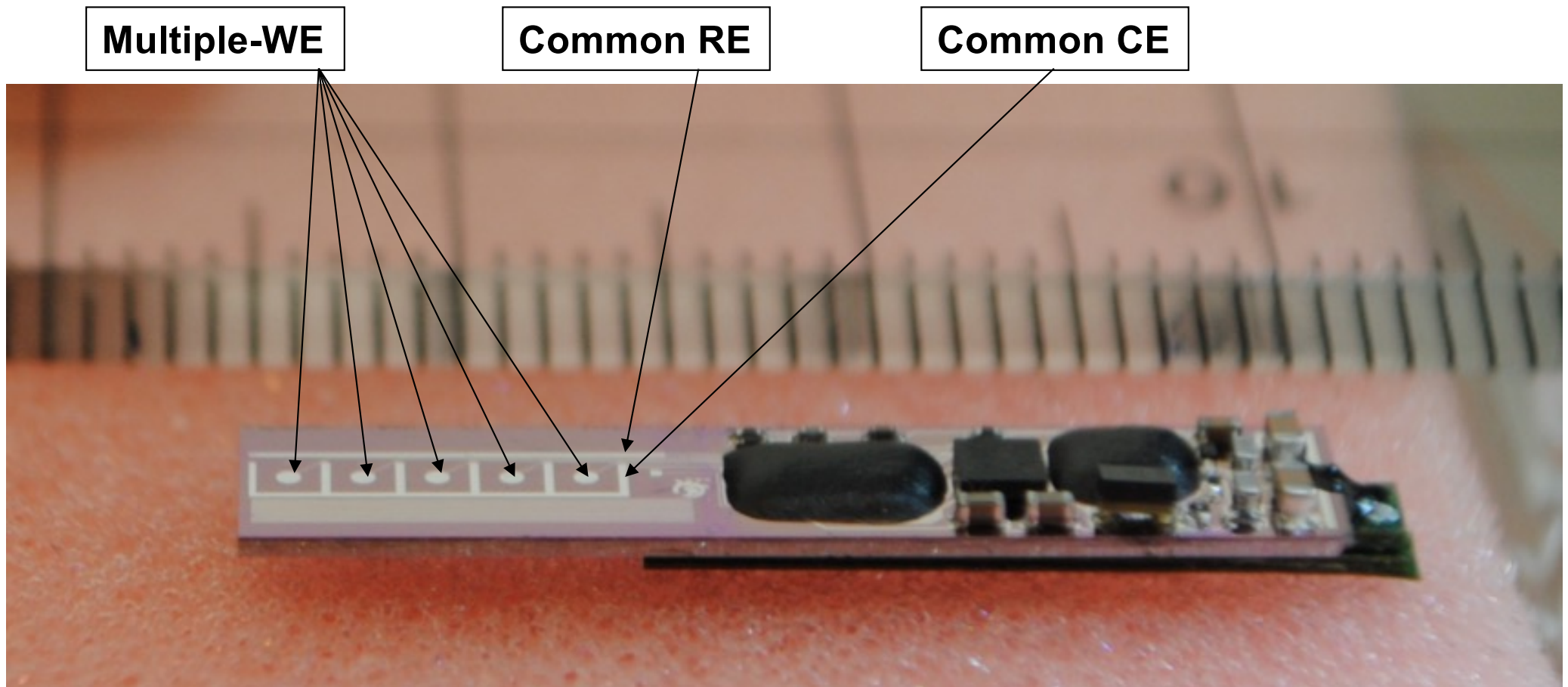
E. 5

F. 5+

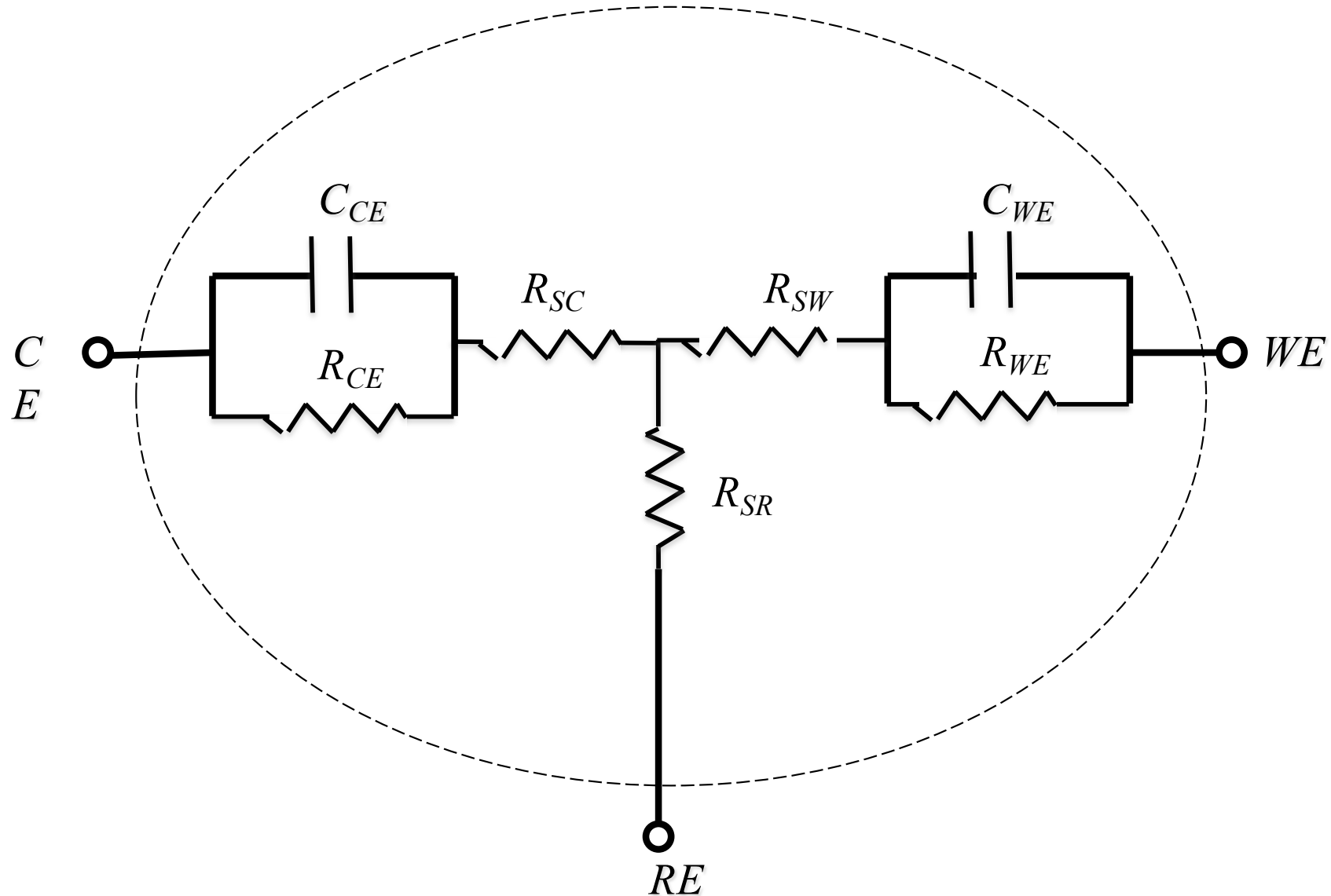
The three-electrode Electrochemical cells



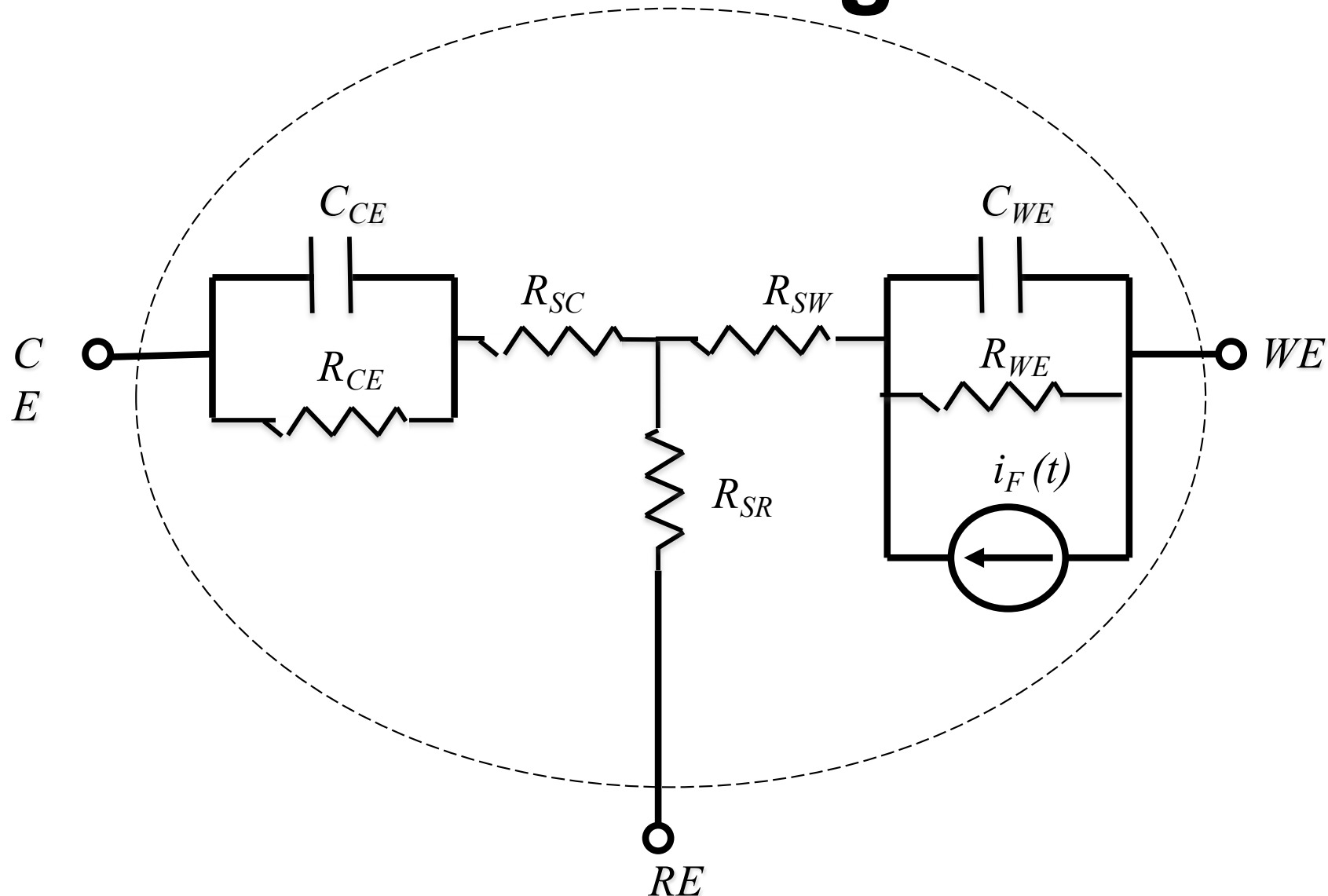
Electrochemical cells with multiple-electrodes



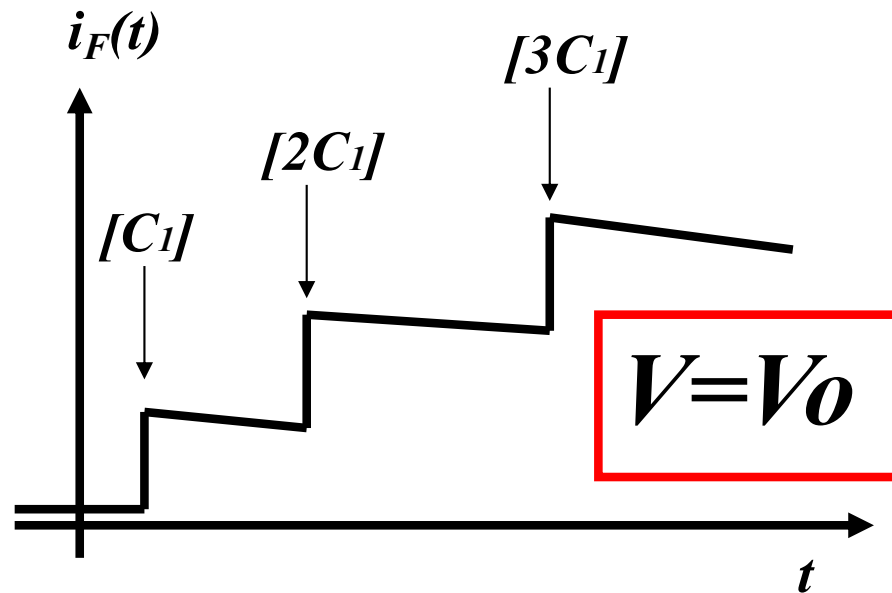
Equivalent circuit



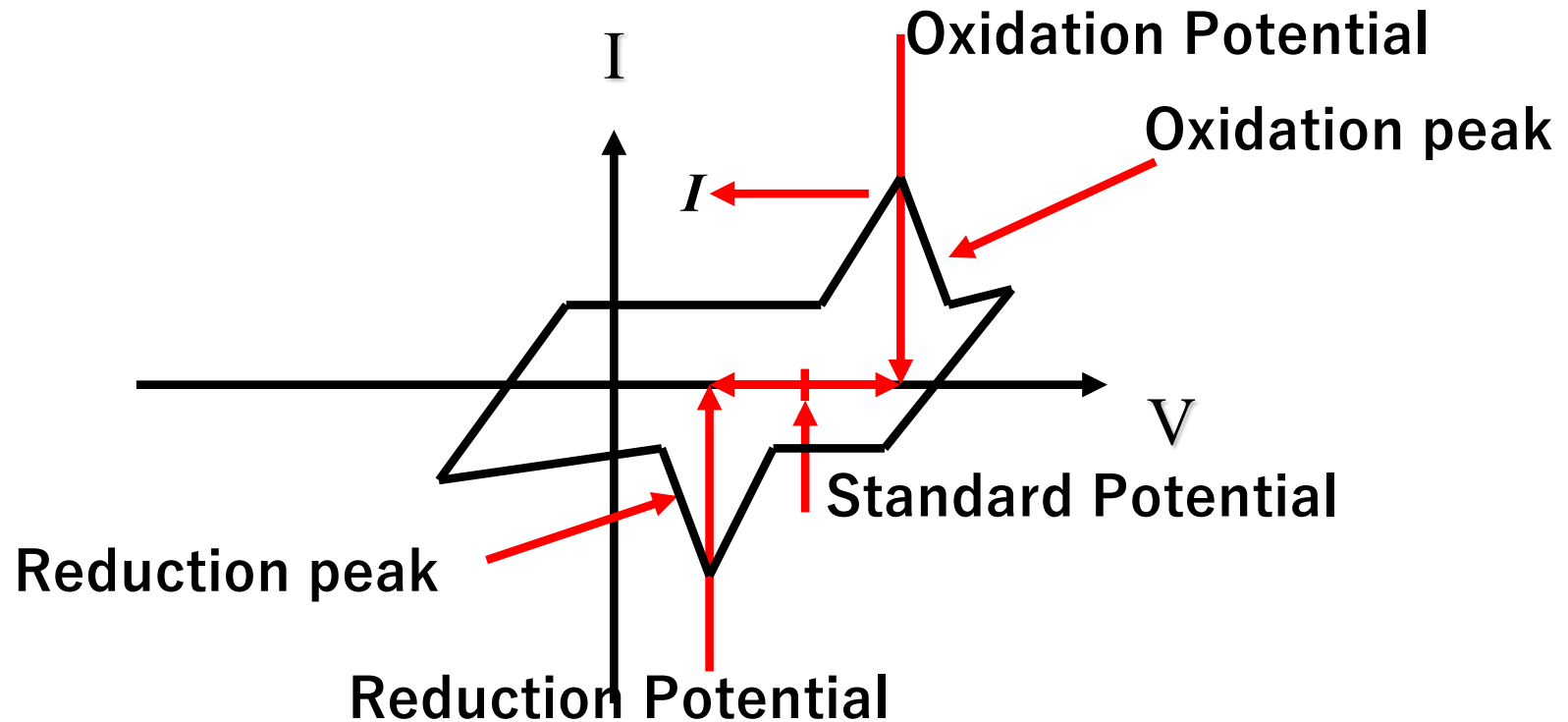
Equivalent circuit with Faradaic current-generator



Faradaic currents from Crono-Amperometry

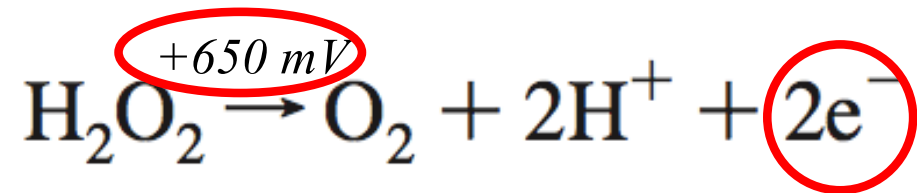


Faradaic currents from Cyclic Voltammetry

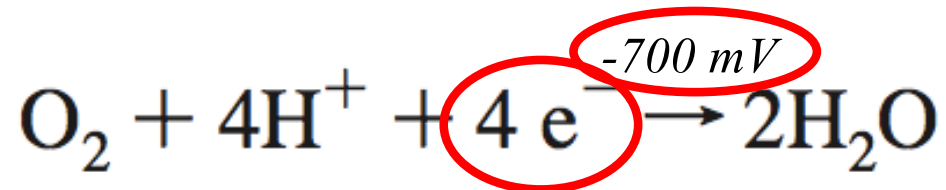


Redox with oxidases

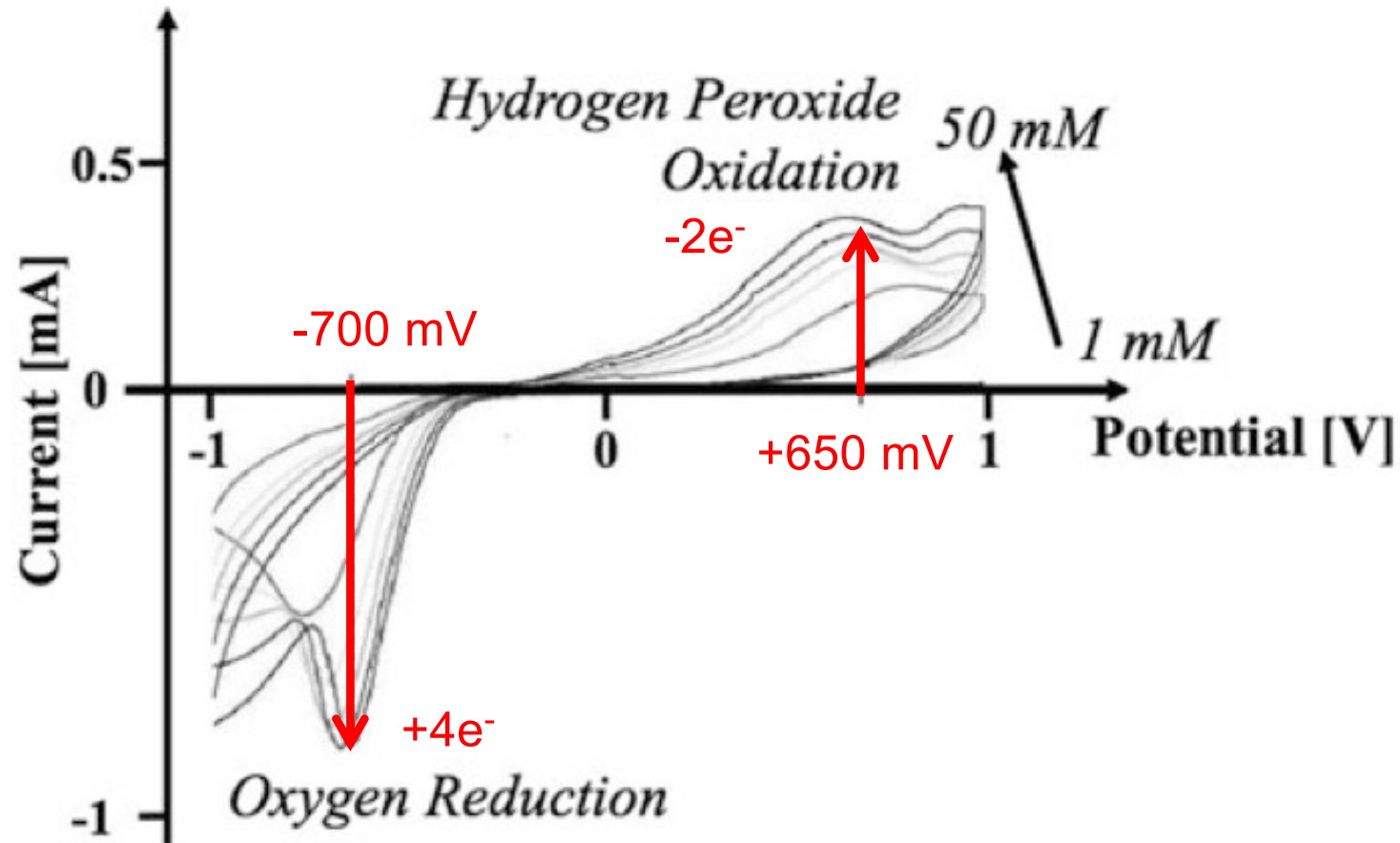
The hydrogen peroxide provides two possible redox reactions.
An oxidation:



And a reduction (of the oxygen):



Redox with hydrogen peroxide



O_2 reduction and H_2O_2 oxidation observed by potential sweeping

Relevant Redox Reactions Equations?

$$V_{I_{MAX}} = f([C]) \quad \text{Nernst equation}$$

$$I = f([C], V) \bigg|_{\frac{dV}{dt} \neq 0} \quad \text{Randles-Sevcik equation}$$

$$I = f([C], t) \big|_{V=Const} \quad \text{Cottrell equation}$$



Q7

What is the Laplace Transform?

- A. An integral transform only for periodical functions
- B. An integral transform only for converging functions
- ☒ C. An integral transform only for non-converging functions
- ☒ D. An integral transform to simplify differential equations

To derive electrochemical Equations we need of the Laplace' s Transforms

$$F(s) = L_s[f(t)] = \hat{f}(s) = \int_0^{+\infty} f(t)e^{-st} dt$$

$$L_s[af(t) + bg(t)] = aL_s[f(t)] + bL_s[g(t)] = a\hat{f}(s) + b\hat{g}(s)$$

$$L_s[t^n] = \frac{n!}{s^{n+1}}$$

$$L_s\left[\frac{\partial f(t)}{\partial t}\right] = s\hat{f}(s) - f(0)$$

$$L_s\left[\frac{\partial^2 f(t)}{\partial t^2}\right] = s^2 \hat{f}(s) - s f(0) - \left[\frac{\partial f(t)}{\partial t}\right]_{t=0}$$

Flick's Laws

The mass flow also has a direction driven by the gradient of concentration (defined by means of the vector differential operator):

$$\vec{j}_m = -D \vec{\nabla} C(\vec{x}, t)$$

In non-vector form (by rotating the x-axis in the direction of the maximum flux and neglecting the variations on y- and z-axes):

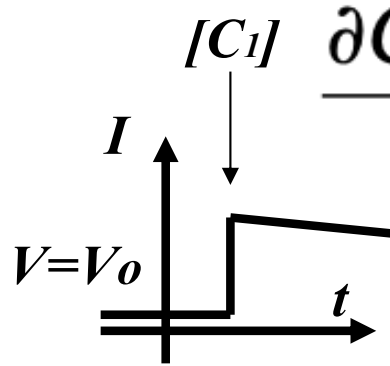
$$j_m \cong -D \frac{\partial C(x, t)}{\partial x}$$

The accumulation rate is provided by the mass flux through a fluidic volume:

$$\frac{\partial C(x, t)}{\partial t} = - \frac{\partial j_m}{\partial x} \rightarrow \frac{\partial C(x, t)}{\partial t} = D \frac{\partial^2 C(x, t)}{\partial x^2}$$

The Cottrell Equation

Linear diffusion equation



$$\frac{\partial C(x,t)}{\partial t} = D \frac{\partial^2 C(x,t)}{\partial x^2}$$

$$L_s \left[\frac{\partial f(t)}{\partial t} \right] = s\hat{f}(s) - f(0)$$

Boundary conditions

$$\left\{ \begin{array}{l} C(x,0) = C_o \\ \lim_{x \rightarrow \infty} C(x,t) = C_o \\ C(0,t) = 0, t \rightarrow \infty \end{array} \right.$$

$$s\hat{C}_0(x,s) - C(x,0) = D \frac{\partial \hat{C}_0(x,s)}{\partial x^2}$$

$$C(x,0) = C(x \rightarrow \infty, t) = C_o$$

$$\frac{\partial^2 \hat{C}(x,s)}{\partial x^2} - \frac{s}{D} \hat{C}(x,s) = -\frac{C_o}{D}$$

The Cottrell Equation

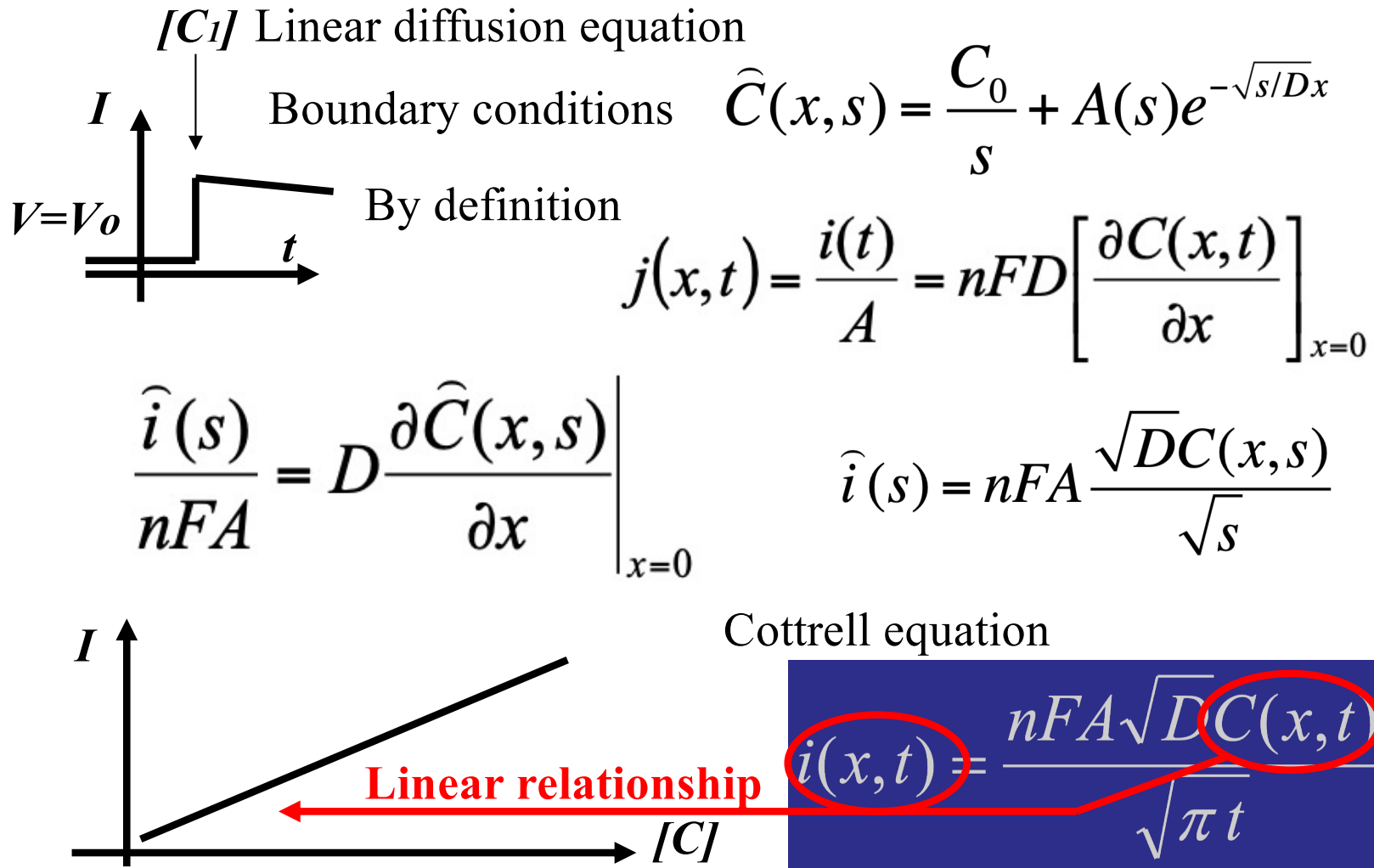
$$\frac{\partial^2 \hat{C}(x, s)}{\partial x^2} - \frac{s}{D} \hat{C}(x, s) = -\frac{C_0}{D}$$

$$\hat{C}(x, s) = \frac{C_0}{s} + A(s)e^{-\sqrt{s/D}x} + B(s)e^{+\sqrt{s/D}x}$$

$$\boxed{\begin{aligned} \lim_{x \rightarrow \infty} C(x, t) &= C_0 \\ L_s[t^n] &= \frac{n!}{s^{n+1}} \end{aligned}} \longrightarrow \lim_{x \rightarrow \infty} \hat{C}(x, s) = \frac{C_0}{s}$$

$$B(s) = 0, \text{ while } \hat{C}(x, s) = \frac{C_0}{s} + A(s)e^{-\sqrt{s/D}x}$$

The Cottrell Equation





Q8

$$i(x,t) = \frac{nFA\sqrt{DC(x,t)}}{\sqrt{\pi t}}$$

What is the “A” in the Cottrell Equation?

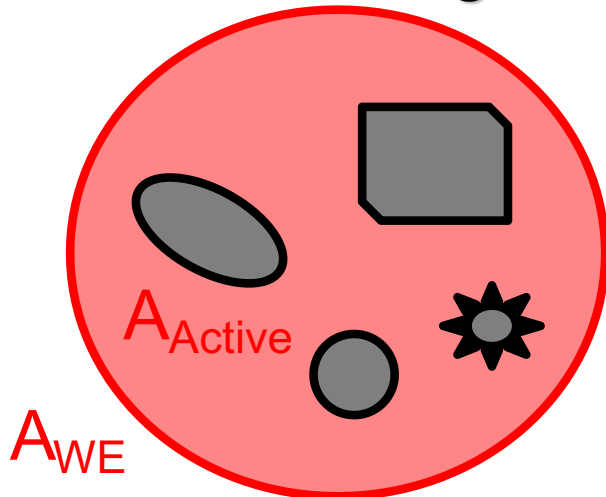
- A. The geometrical area of the WE
- ☒ B. The active area of the WE
- C. The geometrical area of the CE
- D. The active area of the CE
- E. The geometrical area of the RE
- F. The active area of the RE

Geometrical Area vs Active Area

$$i(x,t) = \frac{nFA\sqrt{DC(x,t)}}{\sqrt{\pi t}}$$

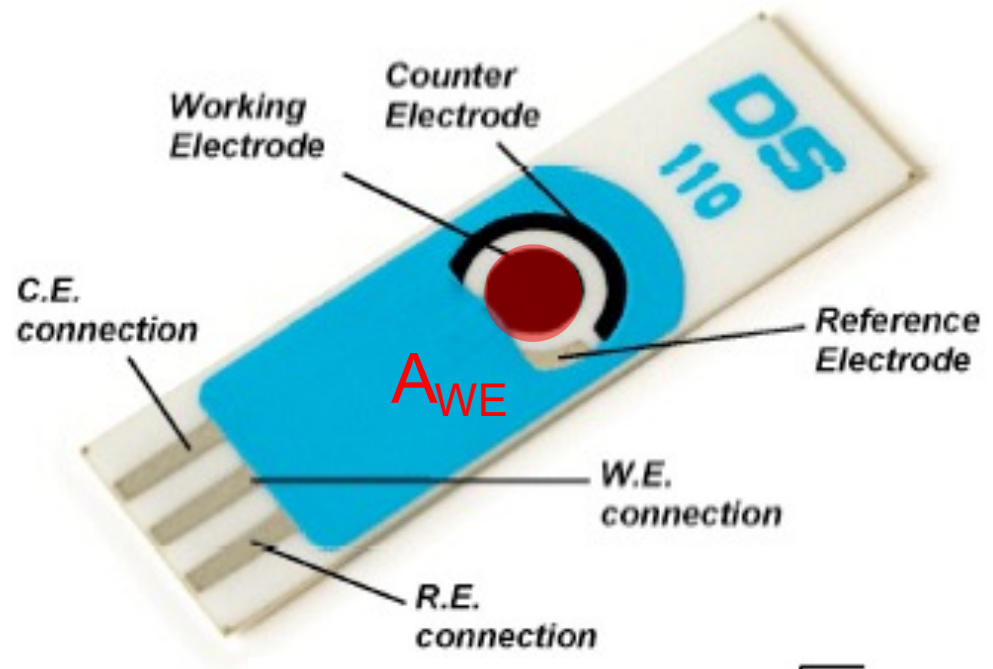
?

Non Active Regions



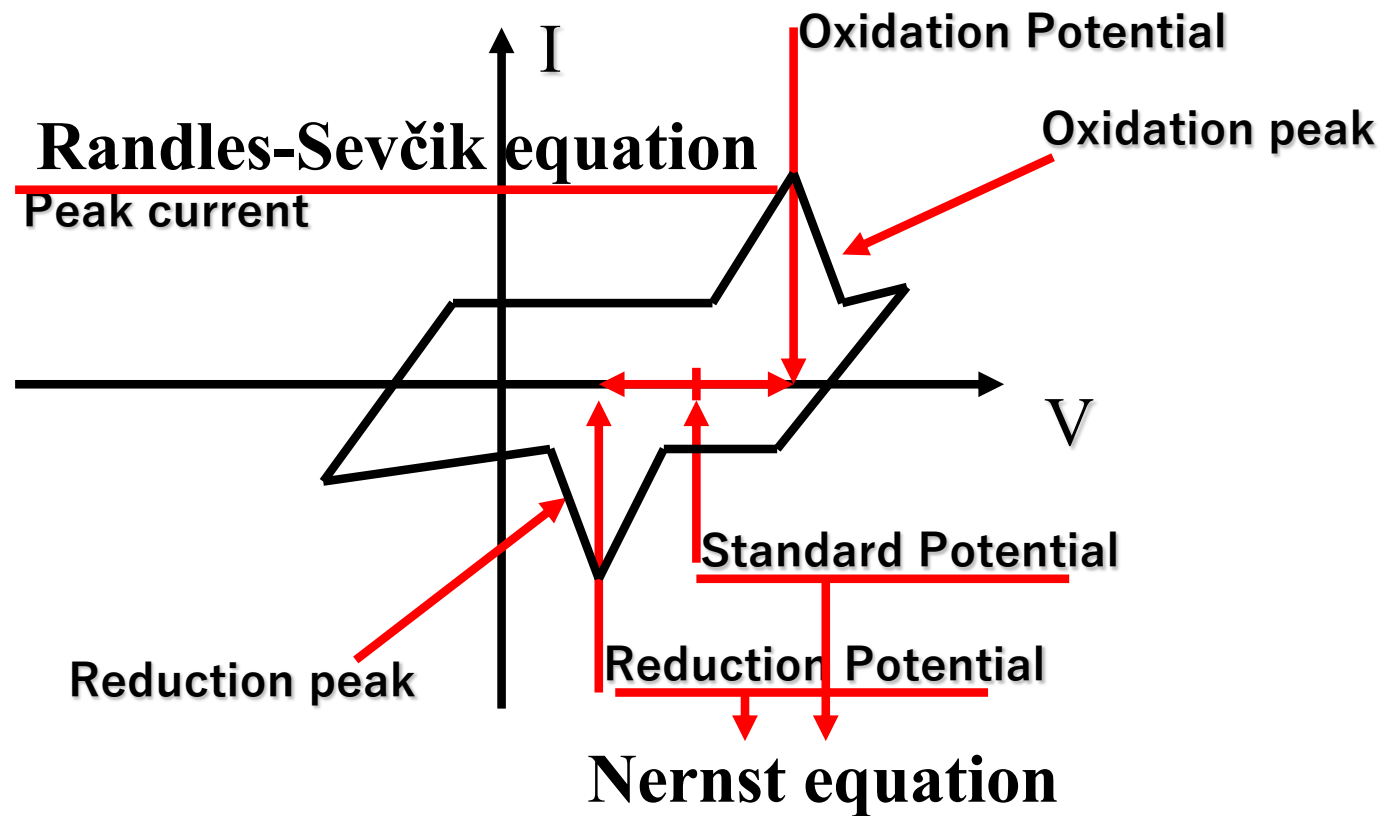
$$A_{Active} < A_{WE}$$

Electrochemically Active Area



$$i(x,t) = \frac{nFA_{Active}\sqrt{DC(x,t)}}{\sqrt{\pi t}}$$

Redox reactions from Voltammetry





Q9

What is the meaning of the “Oxidation Potential”?

- A. The Energy of the current generated at the WE
- B. The Energy of the current collected at the CE
- ☒ C. The Energy provided by the RE
- D. The Energy required by the Oxidation-reaction
- E. A reference potential due to materials used for the RE



Q10

What is the meaning of the “Standard Potential”?

- A. The Energy of the current generated at the WE
- B. The Energy of the current collected at the CE
- C. The Energy provided by the RE
- D. The Energy required by the Oxidation-reaction
- ☒ E. A reference potential due to materials used for the RE

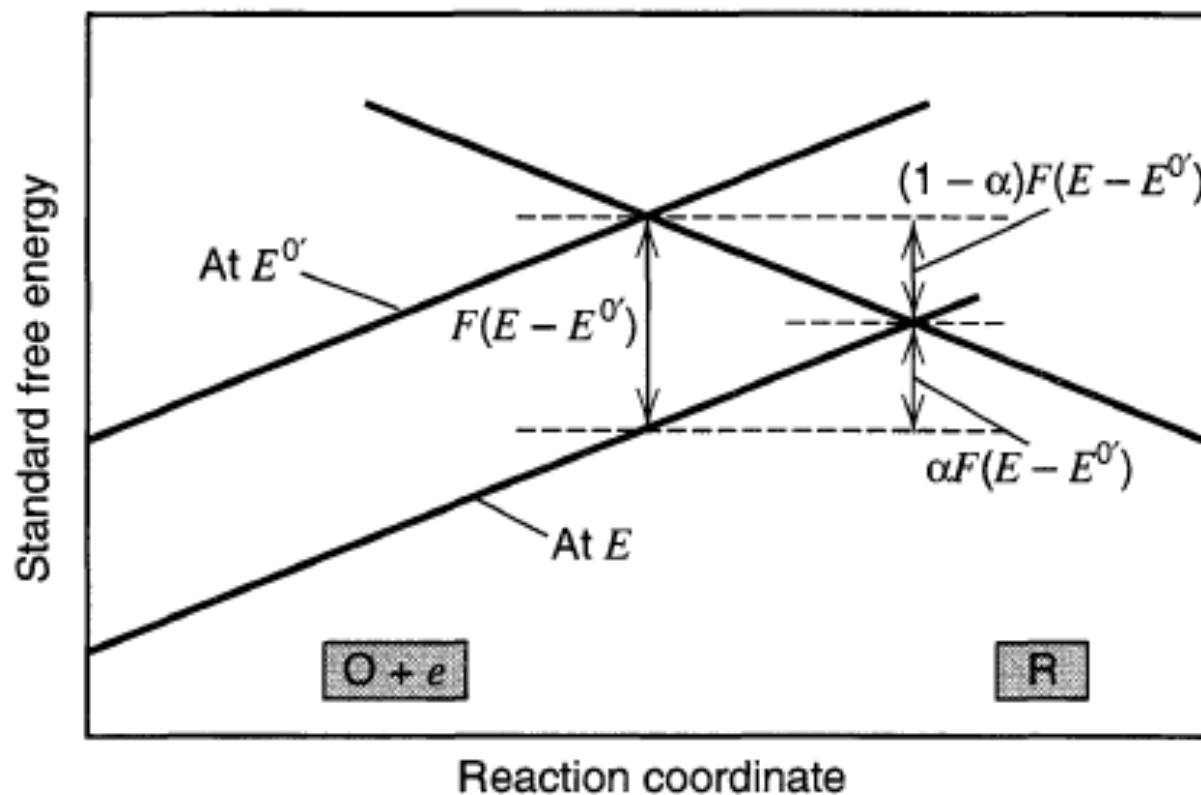


Q11

What is the meaning of the difference between “Standard” and “Oxidation” Potential?

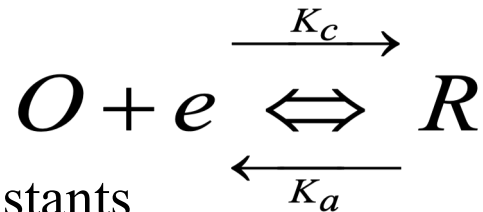
- A. The Energy of the current generated at the WE
- B. The Energy of the current collected at the CE
- C. The Energy provided by the RE
- ☒ D. The Energy required by the Oxidation-reaction
- E. A reference potential due to materials used for the RE

Redox Reactions



Nernst Equation

Redox Reaction



Equilibrium Constants

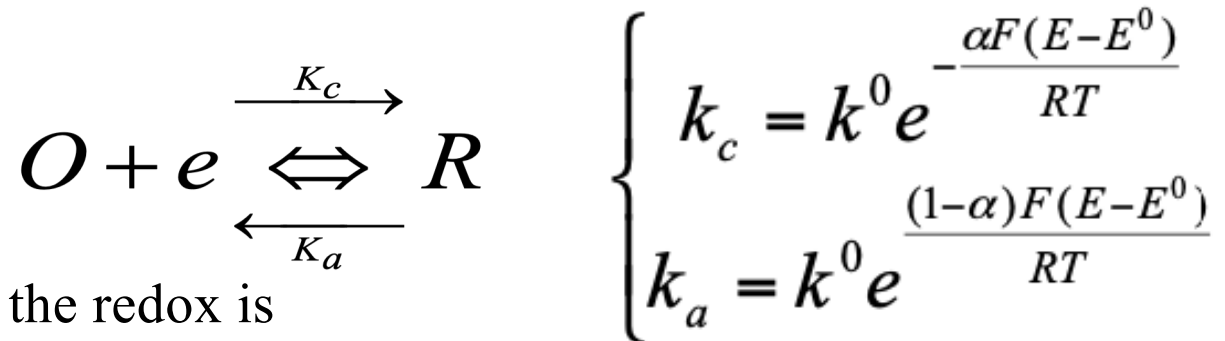
$$\begin{cases} k_c = k_c^0 e^{-\frac{\Delta G_c}{RT}} = k_c^0 e^{-\frac{\Delta G_c^0 + \alpha F(E-E^0)}{RT}} \\ k_a = k_a^0 e^{-\frac{\Delta G_a}{RT}} = k_a^0 e^{-\frac{\Delta G_a^0 - (1-\alpha)F(E-E^0)}{RT}} \end{cases} = \boxed{\begin{cases} k_c^0 e^{-\frac{\Delta G_c^0}{RT}} e^{-\frac{\alpha F(E-E^0)}{RT}} \\ k_a^0 e^{-\frac{\Delta G_a^0}{RT}} e^{-\frac{(-1+\alpha)F(E-E^0)}{RT}} \end{cases}}$$

@ Equilibrium:

$$E = 0; \alpha = 0.5; k_c = k_a \Rightarrow k_c^0 e^{-\frac{\Delta G_c^0}{RT}} = k_a^0 e^{-\frac{\Delta G_a^0}{RT}} = k^0$$

Nernst Equation

Redox Reaction



The current from the redox is

$$i = i_c - i_a = nFA[k_c C_O(0,t) - k_a C_R(0,t)]$$

$$i = FAk^0 \left[C_O(0,t) e^{-\frac{\alpha F(E-E^0)}{RT}} - C_R(0,t) e^{\frac{(1-\alpha)F(E-E^0)}{RT}} \right]$$

@ Equilibrium:

$$i = 0 \Rightarrow C_O(0,t) e^{-\frac{\alpha F(E-E^0)}{RT}} = C_R(0,t) e^{\frac{(1-\alpha)F(E-E^0)}{RT}}$$

Nernst Equation

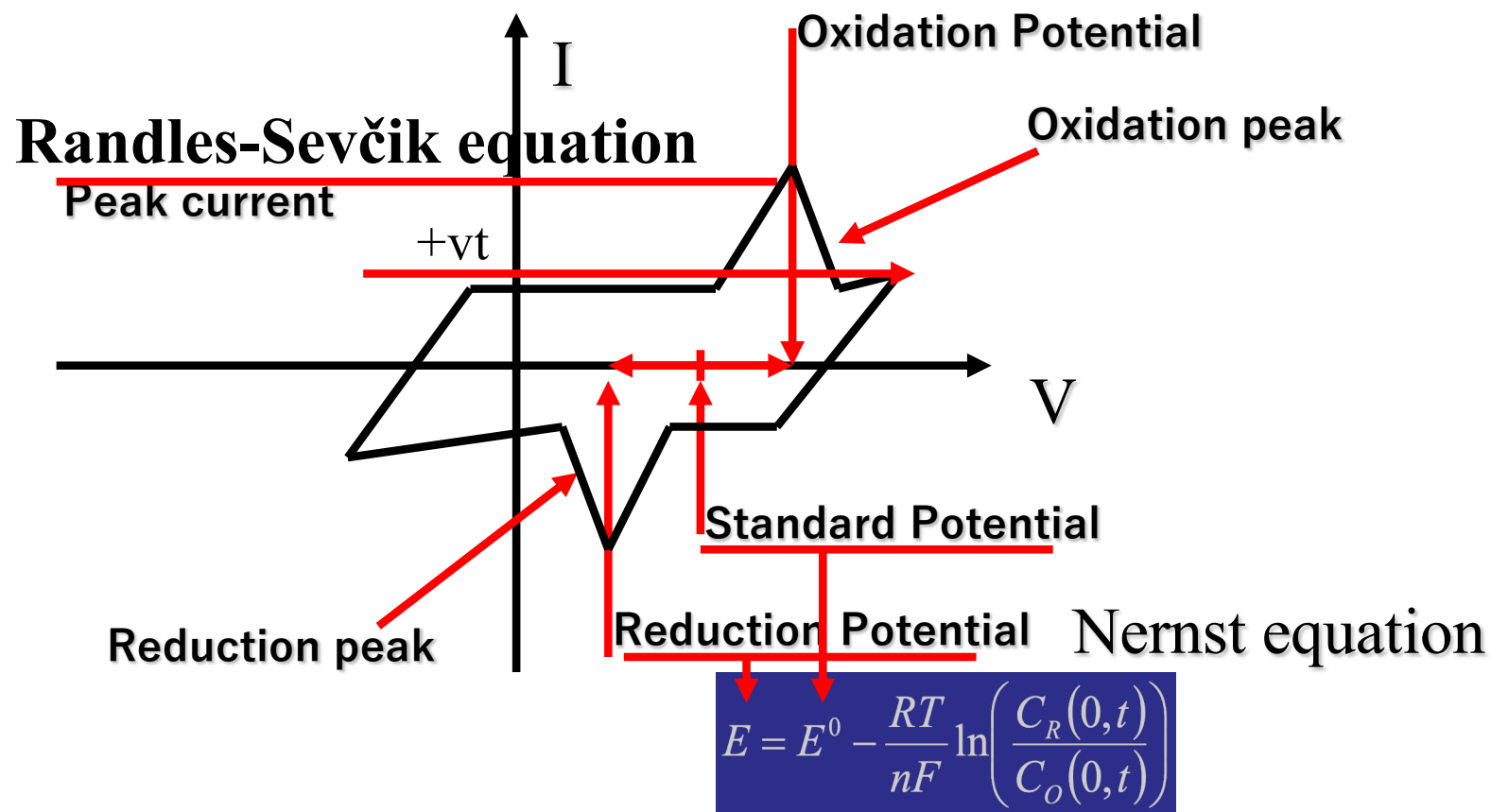
@ Equilibrium:

$$i = 0 \Rightarrow C_o(0,t)e^{-\frac{\alpha F(E-E^0)}{RT}} = C_R(0,t)e^{\frac{(1-\alpha)F(E-E^0)}{RT}}$$
$$i = 0 \Rightarrow \frac{C_o(0,t)}{C_R(0,t)} = e^{\frac{F(E-E^0)}{RT}} \Rightarrow \frac{F(E-E^0)}{RT} = \ln \left[\frac{C_o(0,t)}{C_R(0,t)} \right]$$

$$E = E^0 + \frac{RT}{nF} \ln \left[\frac{C_o(0,t)}{C_R(0,t)} \right] \text{Nernst equation}$$

If n electrons are involved!

Redox reactions from Voltammetry



Randles-Sevcik Equation

Voltage Sweep

$$E = E_i + \nu t$$

$$\frac{C_o(0,t)}{C_R(0,t)} = e^{\frac{F(E+\nu t-E^0)}{RT}}$$

$$\hat{C}_0(x,s) = \frac{C_0}{s} + A(s)e^{-\sqrt{s/D}x}$$

$$j(x,t) = \frac{i(t)}{A} = nFD \left[\frac{\partial C(x,t)}{\partial x} \right]_{x=0} \Rightarrow i(t) = nFAD \left[\frac{\partial C(x,t)}{\partial x} \right]_{x=0}$$

$$\left[\frac{\partial C(x,t)}{\partial x} \right]_{i=i_{peak}} \propto \sqrt{\frac{nFD\nu}{RT}} C(0,t) \Rightarrow i(t) = nFAD \sqrt{\frac{nFD\nu}{RT}} C(0,t)$$

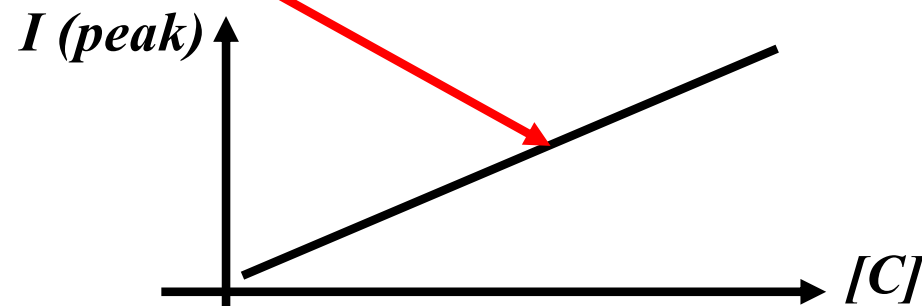
Randles-Sevčik Equation

Voltage Sweep

$$E = E_i + \nu t$$

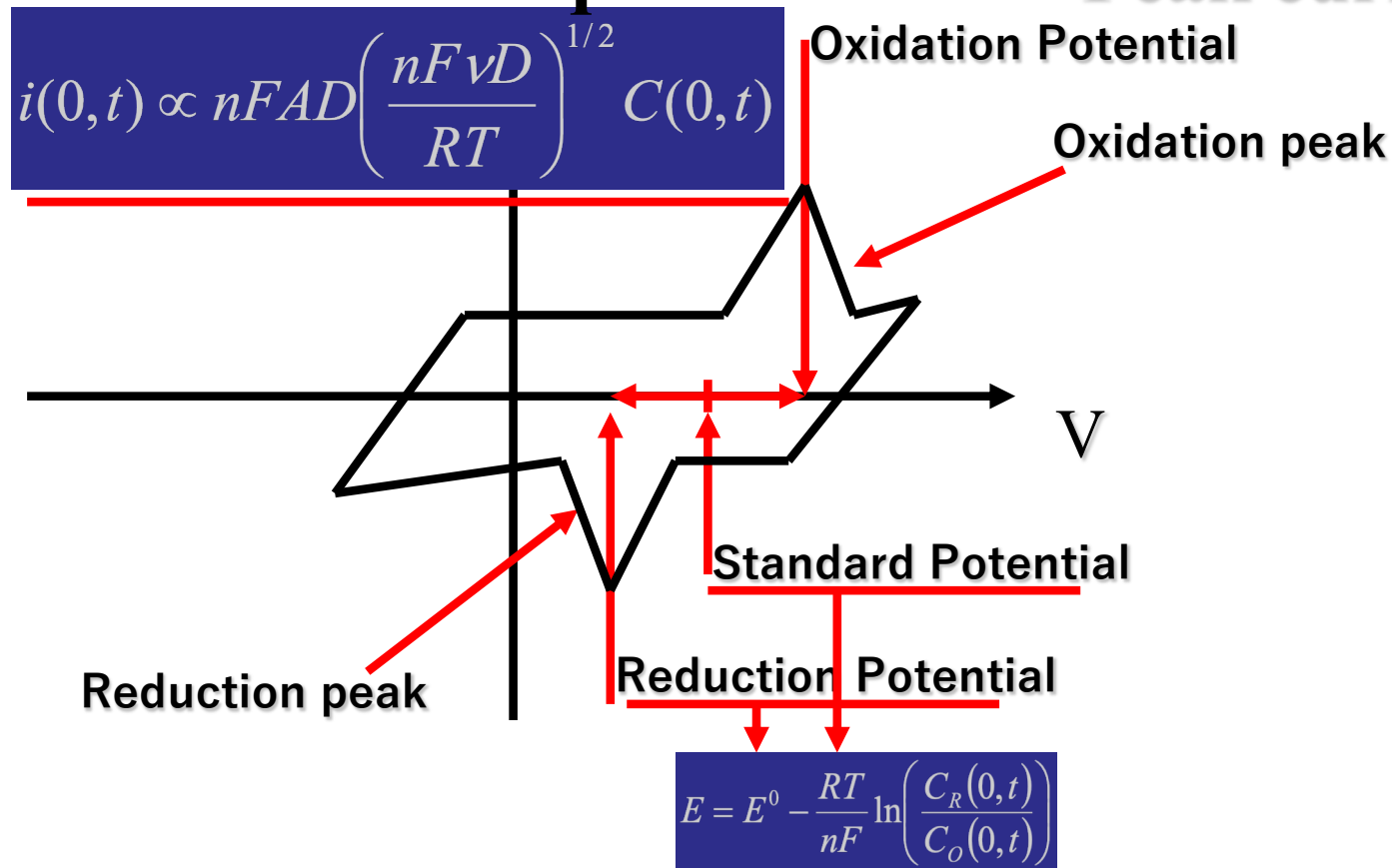
$$\frac{C_o(0,t)}{C_R(0,t)} = e^{\frac{F(E+\nu t-E^0)}{RT}}$$

$$i(t) = nFAD \sqrt{\frac{nFD\nu}{RT}} C(0,t)$$



Redox reactions from Voltammetry

Randles-Sevcik equation for the Peak current



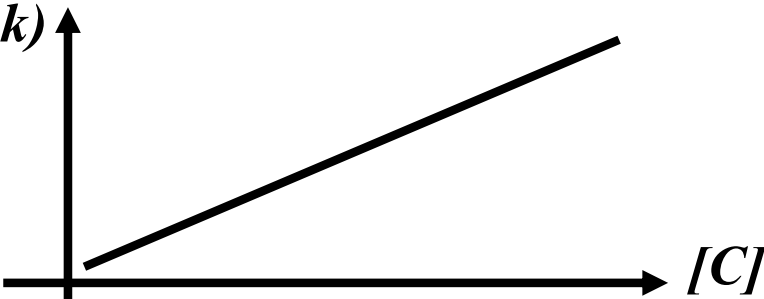
Nernst equation

Detection Principle

- Sensitivity: definition

$$i(t) = nFAD\sqrt{\frac{nFD\nu}{RT}} C(0,t)$$

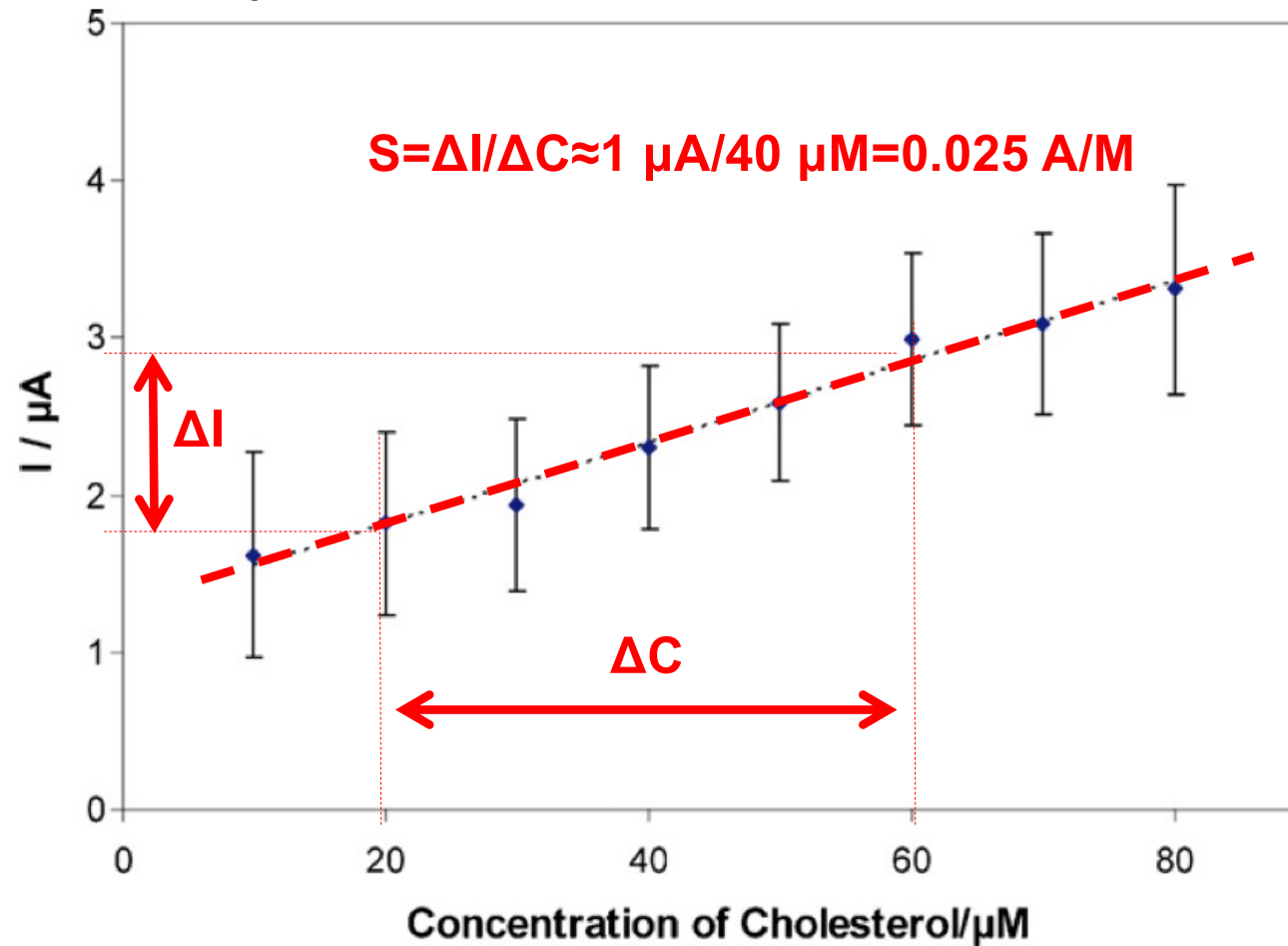
I (peak)


$$\Delta i = nFAD\sqrt{\frac{nFD\nu}{RT}} \Delta C \rightarrow \frac{\Delta i}{\Delta C} \equiv S$$

Detection Sensitivity!

Detection Principle

- Sensitivity: example – A linear sensor





Q12

In biosensing, is 25 mA/M fully equivalent to $25 \text{ nA}/\mu\text{M}$?

- A. Yes, since it is mathematically correct
- B. Yes, since units are equivalent
- C. In some cases, depending on the kind of sensing
- ☒ D. No, since units matter
- E. No, since it is not mathematically correct

Detection Principle

- Sensitivity: metric considerations

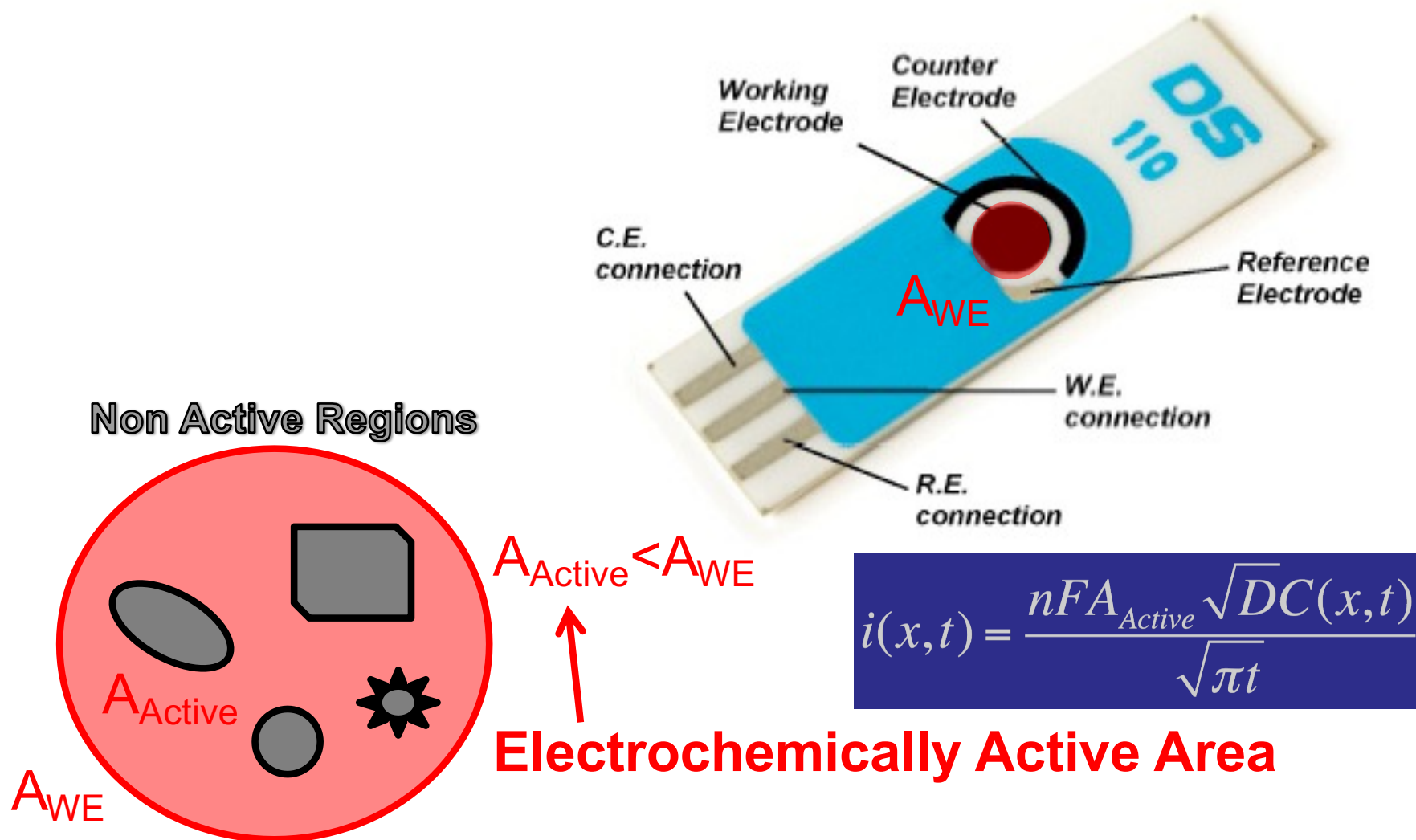
$$S = \frac{\Delta i}{\Delta C} = \frac{1 \mu A}{40 \mu M} = 25 \frac{mA}{M}$$

Mathematically correct, but are we going to measure mAmpere each Molar of concentration?

$$S = \frac{\Delta i}{\Delta C} = \frac{1 \mu A}{40 \mu M} = 25 \frac{nA}{\mu M}$$

More correct, because we are going to require a precision of sub- μ Ampere meanwhile facing variations on μ M range

Geometrical Area vs Active Area



Detection Principle

- Sensitivity: metric considerations

$$S = \frac{\Delta i}{\Delta C} = \frac{1 \mu A}{40 \mu M} = 25 \frac{mA}{M}$$

Correct, but we cannot compare biosensors with different geometry on working electrodes

$$S_A = \frac{\Delta i}{\Delta C \cdot A} = \frac{1 \mu A}{40 \mu M \cdot 0.2 cm^2} = 125 \frac{nA}{\mu M \cdot cm^2}$$

More useful to compare biosensors with different geometry on working electrodes



Q13

$$S_A = \frac{\Delta i}{\Delta C \cdot A}$$

What is the “A” in the definition of S_A ?

- A.** The geometrical area of the WE
- B. The active area of the WE
- C. The geometrical area of the CE
- D. The active area of the CE
- E. The geometrical area of the RE
- F. The active area of the RE

Sensitivity per Unit Area

$$S = \frac{\Delta i}{\Delta C} \quad \text{Sensitivity}$$

$$S_A = \frac{S}{A_{WE}} \quad \text{Sensitivity per unit of Area}$$

$$S_A = \frac{\Delta i}{A_{WE} \Delta C} = \frac{nFA_{Active} \sqrt{D}}{A_{WE} \sqrt{\pi t}} \xrightarrow{A_{Active} \rightarrow A_{WE}} \frac{nF \sqrt{D}}{\sqrt{\pi t}}$$



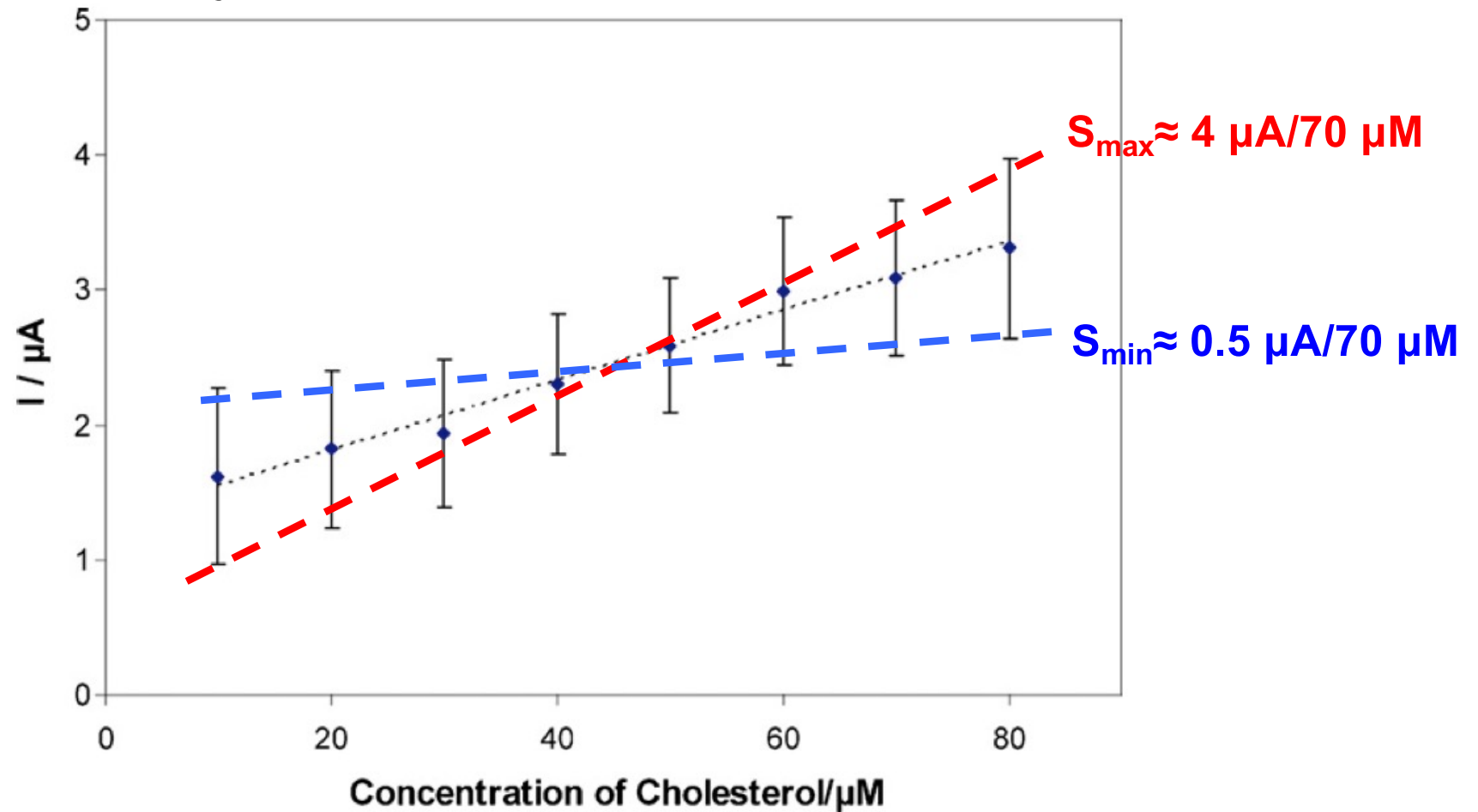
Q14

Does the S need to be estimated with standard deviation?

- A. Not at all !!!
- B. No, since S is calculated by a linear regression
- C. In some cases, when measures are very noisy
- D. Yes, but not when measures are not so noisy
- ☒ E. Yes, of course!!!

Detection Principle

- Sensitivity: Measurement errors



Detection Principle

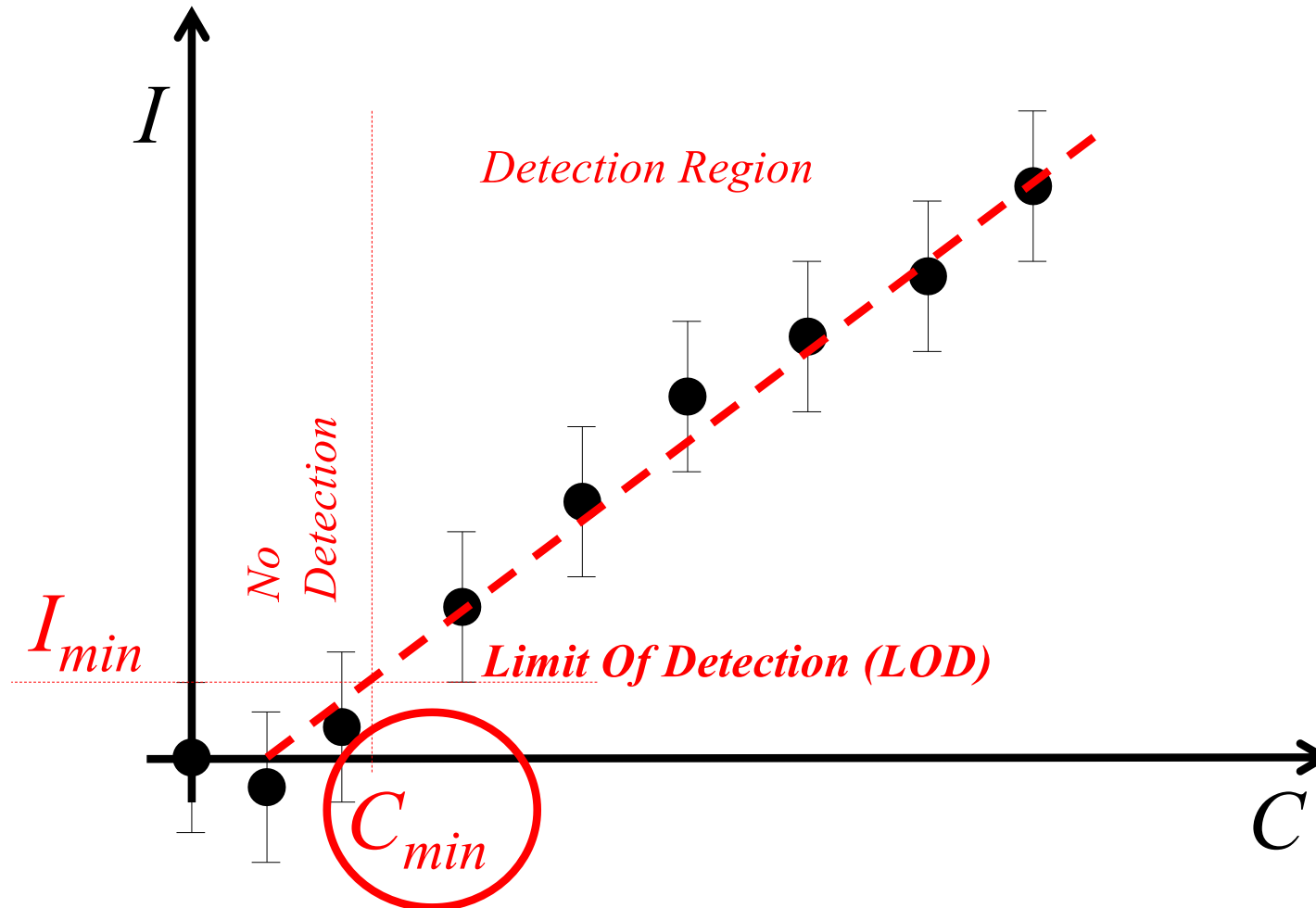
- Sensitivity: Average value and standard its deviation

$$\left. \begin{aligned} S_{\max} &\approx \frac{4 \mu A}{70 \mu M} = 57 \frac{nA}{\mu M} \\ S_{\min} &\approx \frac{0.5 \mu A}{70 \mu M} = 7 \frac{nA}{\mu M} \end{aligned} \right\} \rightarrow \bar{S} = 32 \pm 25 \frac{nA}{\mu M}$$

More correct, because we have measurement errors that do not allow a precise estimation of the sensitivity

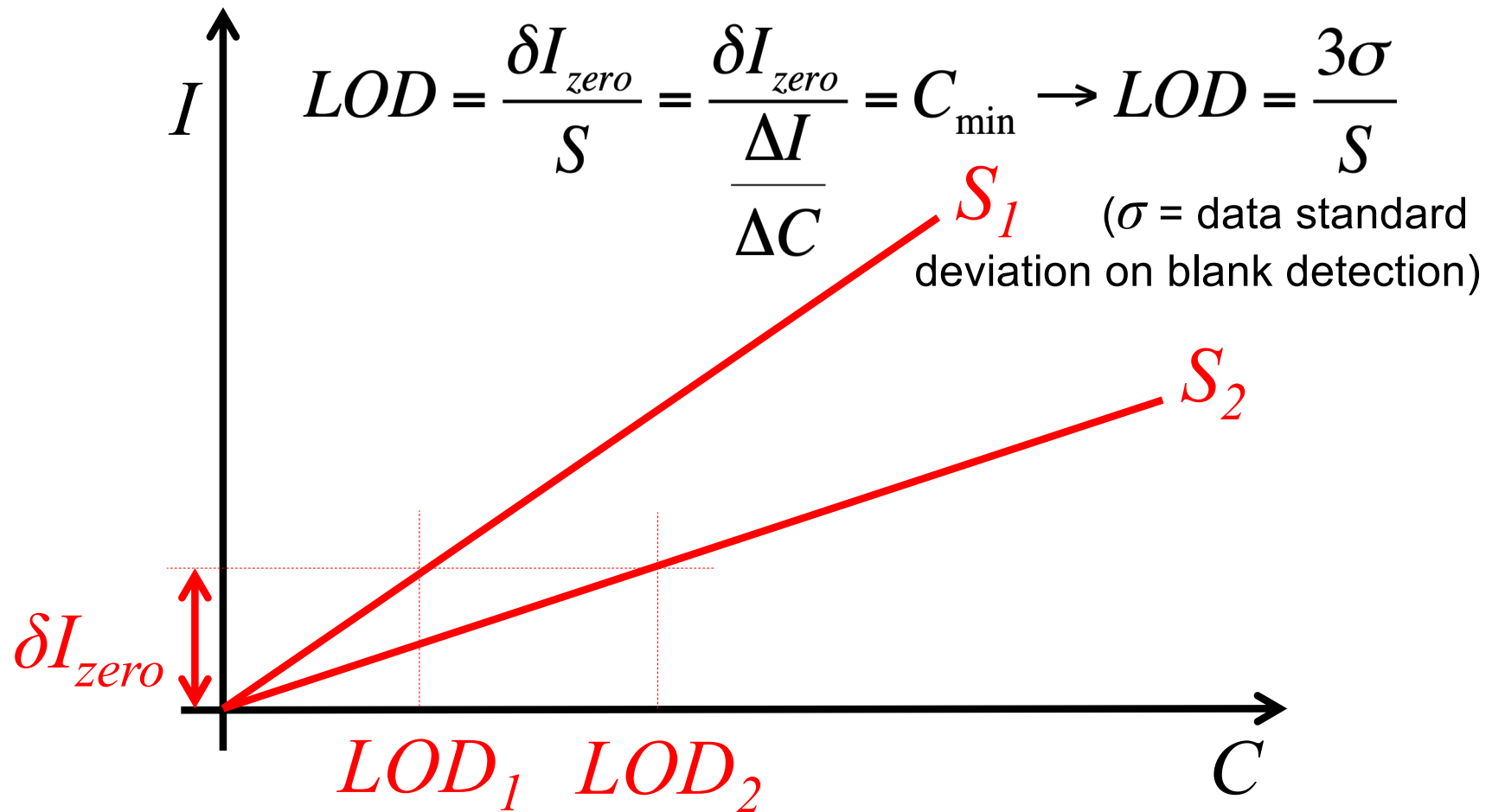
Detection Principle

- Detection Limit: a graphic interpretation



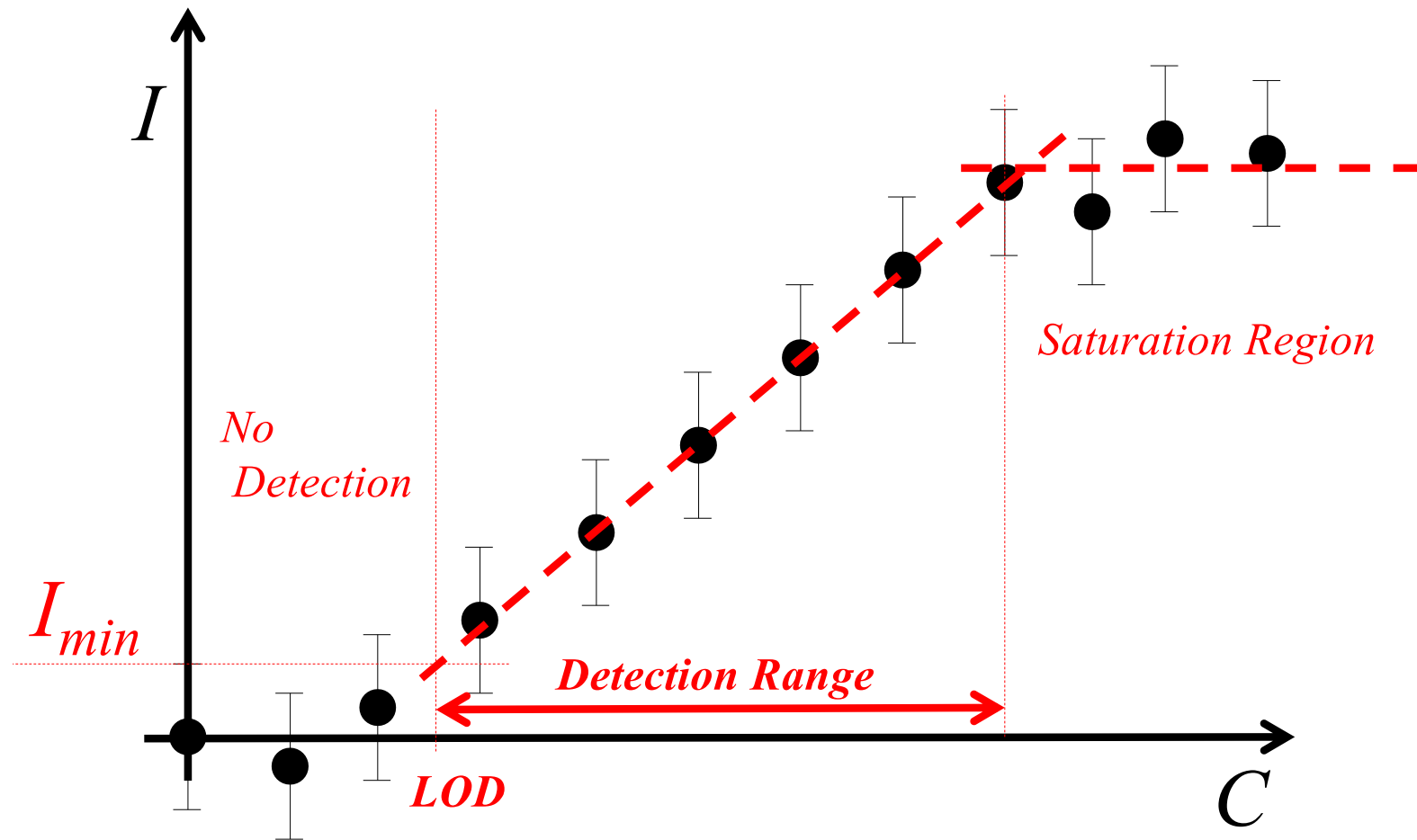
Detection Principle

- Detection Limit: a precise definition



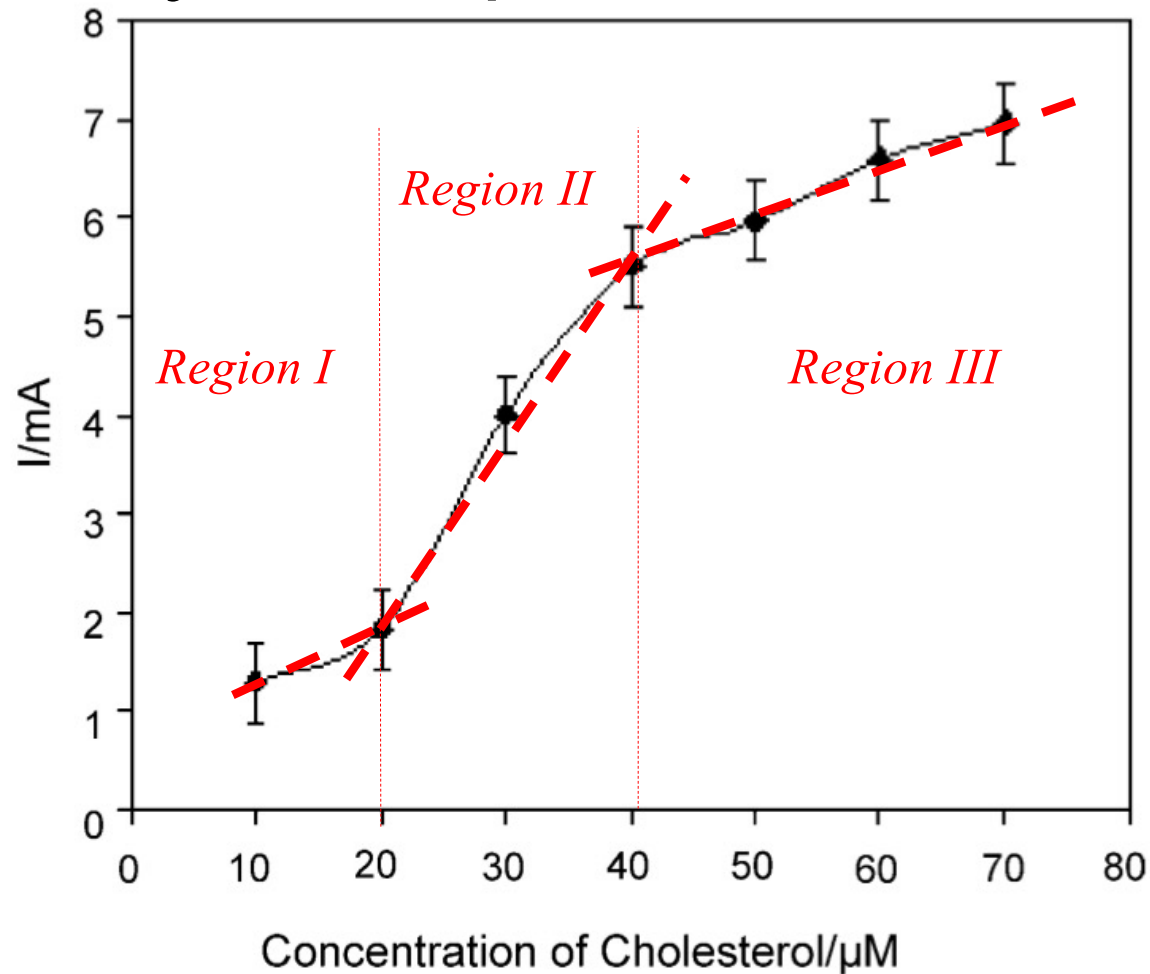
Detection Principle

- Saturation region: a graphic interpretation



Detection Principle

- Sensitivity: example – A non linear sensor



Sensitivity

- The Clarke's Error Grid

